Benchmarking the Pure Random Search on the BBOB-2009 Noisy Testbed

Anne Auger TAO Team - INRIA Saclay LRI, Bat 490, Univ. Paris-Sud 91405 Orsay Cedex, France anne.auger@inria.fr

ABSTRACT

We benchmark the Pure-Random-Search algorithm on the BBOB 2009 noisy testbed. Each candidate solution is sampled uniformly in $[-5, 5]^D$, where *D* denotes the search space dimension. The maximum number of function evaluations chosen is 10^6 times the search space dimension. With this budget the algorithm is not able to solve any single function of the testbed.

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization, Global Optimization, Unconstrained Optimization; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

Algorithms

Keywords

Benchmarking, Black-box optimization, Evolutionary computation, Pure random search, Monte-Carlo

1. INTRODUCTION

The pure random search proposed by Brooks in 1958 [2] is the most simple stochastic search algorithm. It consists in sampling each search point independently in the search domain and keeping the best solution found.

In this paper, we benchmark the pure random search where each solution is sampled uniformly in $[-5,5]^D$, where D denotes the dimension of the search space. The maximum number of function evaluations is fixed to $10^6 \times D$. The CPU time experiments and implementation details are given in the companion paper [1].

Copyright 2009 ACM 978-1-60558-505-5/09/07 ...\$5.00.

Raymond Ros Univ. Paris-Sud, LRI UMR 8623 / INRIA Saclay, projet TAO F-91405 Orsay, France raymond.ros@Iri.fr

2. RESULTS AND DISCUSSION

Results from experiments according to [4] on the benchmarks functions given in [3, 5] are presented in Figures 1 and 2 and in Tables 1 and 2.

Not too surprisingly, the pure random search cannot solve any function of the testbed. However, the results provide reference results useful for the investigation of more advanced algorithms.

Acknowledgments

We would like to thank Nikolaus Hansen for the way he led the BBOB project, Steffen Finck and Nikolaus Hansen for their great and hard work. We also would like to thank Marc Schoenauer for his kind support and essential help on the C-code.

3. REFERENCES

- A. Auger and R. Ros. Benchmarking the Pure Random Search on the BBOB-2009 Testbed. In Workshop Proceedings of the GECCO Genetic and Evolutionary Computation Conference. ACM, 2009.
- [2] S. H. Brooks. A discussion of random methods for seeking maxima. Operations Research, 6:244–251, 1958.
- [3] S. Finck, N. Hansen, R. Ros, and A. Auger. Real-parameter black-box optimization benchmarking 2009: Presentation of the noisy functions. Technical Report 2009/21, Research Center PPE, 2009.
- [4] N. Hansen, A. Auger, S. Finck, and R. Ros. Real-parameter black-box optimization benchmarking 2009: Experimental setup. Technical Report RR-6828, INRIA, 2009.
- [5] N. Hansen, S. Finck, R. Ros, and A. Auger. Real-parameter black-box optimization benchmarking 2009: Noisy functions definitions. Technical Report RR-6869, INRIA, 2009.

Permission to make digital or hard copies of all or part of this work for personal or classroom use is granted without fee provided that copies are not made or distributed for profit or commercial advantage and that copies bear this notice and the full citation on the first page. To copy otherwise, to republish, to post on servers or to redistribute to lists, requires prior specific permission and/or a fee.

GECCO'09, July 8-12, 2009, Montréal Québec, Canada.



Figure 1: Expected Running Time (ERT, •) to reach $f_{opt} + \Delta f$ and median number of function evaluations of successful trials (+), shown for $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$ (the exponent is given in the legend of f_{101} and f_{130}) versus dimension in log-log presentation. The ERT(Δf) equals to $\#FEs(\Delta f)$ divided by the number of successful trials, where a trial is successful if $f_{opt} + \Delta f$ was surpassed during the trial. The $\#FEs(\Delta f)$ are the total number of function evaluations while $f_{opt} + \Delta f$ was not surpassed during the trial from all respective trials (successful and unsuccessful), and f_{opt} denotes the optimal function value. Crosses (×) indicate the total number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

	f101 in 5-D, N=15, mFE=5.00 e6	f101 in 20-D, N=15, mFE=2.00e7	f102 in 5-D, N=15, mFE=5.00e6	f102 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	Δf # ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}
10	15 1.1e2 7.9e1 1.3e2 1.1e2 15 1.7e4 1.2e4 2.4e4 1.7e4	$0 \ 29e+0 \ 20e+0 \ 32e+0 \ 7.1e6$	10 15 4.6e1 3.6e1 5.7e1 4.6e1	$0 \ 27e+0 \ 20e+0 \ 30e+0 \ 8.9e6$
1e - 1	7 8.5e6 6.2e6 1.5e7 4.1e6		1e-1 6 8.5e6 5.9e6 1.7e7 3.7e6	
$1\mathrm{e}-3$	0 10e-2 41e-3 14e-2 3.2e6		1e-3 0 11e-2 65e-3 17e-2 1.8e6	
1e-5			1e-5	
1e-8			1e-8	
Λf	f_{103} in 5-D, N=15, mFE=5.00e6	f_{103} in 20-D, N=15, mFE=2.00e7 # EBT 10% 90% BT====================================	f_{104} in 5-D, N=15, mFE=5.00e6	f_{104} in 20-D, N=15, mFE=2.00 e7
10	15 6.8e1 5.4e1 8.7e1 6.8e1	$\begin{array}{c} & & \\$	10 14 1.6e6 9.9e5 2.2e6 1.4e6	$0 \ 91e+2 \ 6/e+2 \ 11e+3 \ 1.0e7$
1	15 2.3e4 1.8e4 2.8e4 2.3e4		1 0 $64e^{-1}$ $44e^{-1}$ $90e^{-1}$ 2.0e6	
$1\mathrm{e}-1$	7 8.7e6 6.6e6 1.5e7 4.5e6		1e-1	
1e-3	0 10e-2 36e-3 16e-2 2.0e6		1e-3	
1e-3 1e-8			1e-3	
	f105 in 5-D, N=15, mFE=5.00 e6	f105 in 20-D, N=15, mFE=2.00e7	f106 in 5-D, N=15, mFE=5.00e6	f106 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{succ}$	# ERT 10% 90% RT _{succ}
10	14 2.3e6 1.7e6 2.9e6 2.1e6	0 88e+2 63e+2 11e+3 1.0e7	10 15 1.2e6 9.1e5 1.7e6 1.2e6	0 98e+2 76e+2 11e+3 1.3e7
1	$0 69e-1 36e-1 93e-1 \qquad 2.2e6$		1 0 62e-1 53e-1 88e-1 1.4e6	
1e - 1 1e - 3			1e-1	
1e-5			1e-5	
$1\mathrm{e}-8$			1e-8	
	f_{107} in 5-D, N=15, mFE=5.00 e6	f_{107} in 20-D, N=15, mFE=2.00 e7	f_{108} in 5-D, N=15, mFE=5.00e6	f108 in 20-D, N=15, mFE=2.00 e7
$\frac{\Delta f}{10}$	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{\text{succ}}$	# ERT 10% 90% RT _{succ}
1	15 1.1e4 7.4e3 1.5e4 1.1e4		1 15 2.1e4 1.6e4 2.6e4 2.1e4	
$1\mathrm{e}-1$	9 5.7e6 4.2e6 8.4e6 3.1e6		1e-1 8 6.9e6 5.2e6 9.8e6 3.3e6	
1e - 3	$0 96e-3 54e-3 14e-2 \qquad 2.2e6$		1e-3 0 $98e-3$ $37e-3$ $17e-2$ $3.2e6$	
1e-5			1e-5	
16-3	f_{109} in 5-D. N=15, mFE=5.00e6	f_{100} in 20-D. N=15. mFE=2.00e7	f_{110} in 5-D. N=15. mFE=5.00e6	f110 in 20-D. N=15. mFE=2.00e7
Δf	# ERT 10% 90% RT_{SUCC}	# ERT 10% 90% RT_{SUCC}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{\text{succ}}$	# ERT 10% 90% RT _{SUCC}
10	15 1.2e2 8.9e1 1.5e2 1.2e2	0 28e+0 22e+0 34e+0 1.0e7	10 14 1.8e6 1.3e6 2.3e6 1.4e6	0 80e+2 60e+2 97e+2 7.9e6
1	15 1.8e4 1.4e4 2.3e4 1.8e4		1 0 63e-1 36e-1 90e-1 2.8e6	
1e - 1 1e - 3	10 4.8e6 3.7e6 6.8e6 $3.3e6$		1e-1	
1c - 5 1e - 5			1e-5	
1e-8			1e-8	
1e-8	f111 in 5-D, N=15, mFE=5.00e6	f111 in 20-D, N=15, mFE=2.00e7	le-8	f112 in 20-D, N=15, mFE=2.00e7
$\frac{\Delta f}{10}$	f_{111} in 5-D, N=15, mFE=5.00e6 # ERT 10% 90% RT _{succ}	f_{111} in 20-D, N=15, mFE=2.00e7 # ERT 10% 90% RT _{succ}	$\begin{array}{c} 1e-8 & . & . & . \\ f_{112} \text{ in } 5\text{-}D, \text{ N=15, mFE=5.00e6} \\ \Delta f \ \# \text{ ERT } 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ 10 & 12.20\% \ 12.66 \ 2.7\% \ 10\% \ 1$	f_{112} in 20-D, N=15, mFE=2.00 e7 # ERT 10% 90% RT _{succ}
$\frac{\Delta f}{10}$	$\begin{array}{ccccccc} . & . & . & . & . & . & . & . & . & . $	$ \begin{array}{c} f111 \ \ \mathbf{n} \ \ \mathbf{20\text{-}D}, \ \mathbf{N=}15, \ \mathbf{mFE}=2.00 \ \mathbf{e7} \\ \# \ \ \mathbf{ERT} \ \ 10\% \ \ 90\% \ \ \mathbf{RT}_{\mathrm{succ}} \\ \hline 0 \ \ 94e+2 \ \ 73e+2 \ \ 12e+3 \ \ \ \mathbf{6.3e6} \\ \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} \textbf{f_{112} in 20-D, N=15, mFE=2.00 e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ 0 \ 76e+2 \ 53e+2 \ 95e+2 \ 1.3 e7 \end{array} $
$\frac{\Delta f}{10}$ $\frac{1}{1e-1}$	$ \begin{array}{c} f111 \text{ in 5-D, } N{=}15, \text{ mFE}{=}5.00\text{e6} \\ \# \text{ ERT } 10\% 90\% \text{RT}_{\text{SUCC}} \\ 15 \ 1.4\text{e6} \ 1.1\text{e6} \ 1.8\text{e6} 1.4\text{e6} \\ 0 66e{-}1 46e{-}1 85e{-}1 2.2\text{e6} \\ \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c} & 1112 \text{ in } 20\text{-}\text{D}, \text{ N=15, mFE=2.00e7} \\ \# \text{ ERT } 10\% 90\% \text{ RT}_{\text{succ}} \\ 0 76e+2 53e+2 95e+2 1.3e7 \\ \vdots & \vdots \\ \end{array} $
$\frac{\Delta f}{10}$ $\frac{1}{1e-1}$ $\frac{1e-3}{1e-3}$	$ \begin{array}{c} f111 \ \text{in 5-D}, \ N=15, \ \mathrm{mFE}{=}5.00\mathrm{e6} \\ \# \ \mathrm{ERT} \ 10\% \ 90\% \ \mathrm{RT}_{\mathrm{Succ}} \\ 15 \ 1.4\mathrm{e6} \ 1.1\mathrm{e6} \ 1.8\mathrm{e6} \ 1.4\mathrm{e6} \\ 0 \ 66e{-}1 \ 46e{-}1 \ 85e{-}1 \ 2.2\mathrm{e6} \\ \end{array} $	$\begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15, mFE=2.00 e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\underline{\text{succ}}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3 e6 \\ \vdots & \vdots & \vdots \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} f_{112} \text{ in } 20\text{-}\text{D}, \text{ N=15, mFE=2.00e7} \\ \# \text{ ERT } 10\% 90\% \text{ RT}_{\text{succ}} \\ 0 76e+2 53e+2 95e+2 1.3e7 \\ $
$\frac{\Delta f}{10}$ $\frac{1}{1e-1}$ $\frac{1}{1e-3}$ $\frac{1}{1e-5}$	$ \begin{array}{c} f{111 in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.4e6 \ 1.4e6 \ 1.4e6 \\ 0 \ 66e{-1} \ 46e{-1} \ 85e{-1} \ 2.2e6 \\ \\ \vdots \\ \vdots \\ \end{array} $	$ \begin{array}{c} f111 \text{ in } 20\text{-}D, \text{ N} = 15, \text{ mFE} = 2.00 \text{ e7} \\ \# \text{ ERT } 10\% 90\% \text{ RT}_{\text{succ}} \\ 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3 \text{ e6} \\ \vdots \\ $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \frac{\Delta f}{10} \\ \frac{1}{1e-1} \\ \frac{1e-3}{1e-5} \\ \frac{1e-8}{1e-8} $	f111 in 5-D , N=15, mFE=5.00e6 # ERT 10% 90% RT _{succ} 15 1.4e6 1.1e6 1.8e6 1.4e6 0 66e-1 46e-1 85e-1 2.2e6 	$\begin{array}{c} f_{111} \text{ in } 20\text{-D}, \text{ N=15, mFE=2.00e7} \\ \# \text{ ERT } 10\% 90\% \text{ RT}_{\text{succ}} \\ 0 94e+2 73e+2 12e+3 6.3e6 \\ \vdots \\ $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \frac{\Delta f}{10} \\ \frac{1}{1e-1} \\ \frac{1e-3}{1e-5} \\ \frac{1e-8}{1e-8} \\ \Delta f $	f111 in 5-D, N=15, mFE=5.00 c6 # ERT 10% 90% RT _{succ} 15 1.4 c6 1.8 c6 1.4 c6 0 66e-1 45e-1 8.2 c6 	f111 in 20-D, N=15, mFE=2.00e7 # ERT 10% 90% RT _{succ} 0 94e+2 73e+2 12e+3 6.3e6 f113 in 20-D, N=15, mFE=2.00e7 # ERT 10% 90% RT _{succ}	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \frac{\Delta f}{10} \\ \frac{1}{1e-1} \\ \frac{1e-3}{1e-5} \\ \frac{1e-8}{1e-8} \\ \frac{\Delta f}{10} $	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT & 10\% & 90\% & RT_{succ} \\ 15 \ 1.4e6 & 1.1e6 & 1.8e6 & 1.4e6 \\ 0 & 66e-1 & 46e-1 & 85e-1 & 2.2e6 \\ . & . & . & . \\ . & . & . & . \\ f113 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT & 10\% & 90\% & RT_{succ} \\ 15 \ 1.2e3 \ 8.3e2 \ 1.5e3 & 1.2e3 \\ \end{array} $	$ \begin{array}{c} f111 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \end{array} \\ \\ f113 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ 0 \ 95e+0 \ 73e+0 \ 11e+1 \ 8.9e6 \\ \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\frac{\Delta f}{10}$ $\frac{1}{1e-1}$ $\frac{1}{1e-3}$ $\frac{1}{1e-5}$ $\frac{1}{1e-8}$ $\frac{\Delta f}{10}$ $\frac{1}{1e-1}$	$ \begin{array}{c} f111 \mbox{in 5-D}, \ N=15, \ mFE=5.00 e6 \\ \# \ ERT \ 10\% \ 90\% \ RT_{\rm succ} \\ 15 \ 1.4 e6 \ 1.4 e6 \ 1.4 e6 \\ 0 \ 66e-1 \ 46e-1 \ 85e-1 \ 2.2 e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$		$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\frac{\Delta f}{10}$ $\frac{1}{1e-1}$ $\frac{1}{1e-3}$ $\frac{1}{1e-5}$ $\frac{\Delta f}{10}$ $\frac{1}{1e-1}$ $\frac{1}{1e-3}$	$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \\ 111 \\ \end{array} & {\bf 5-D}, \ N=15, \ mFE=5.00 e6 \\ \end{array} \\ \begin{array}{c} \# \ ERT & 10\% & 90\% & {\rm RT}_{\rm succ} \\ 15 \ 1.4e6 & 1.4e6 & 1.8e6 & 1.4e6 \\ 0 & 66e-1 & 46e-1 & 85e-1 & 2.2e6 \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \end{array} \\ \end{array} $	$ \begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline & & & & & \\ & & & & & \\ & & & & & \\ f113 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9e6 \\ \hline & & & & \\ \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \end{array}$	$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c}$	$ \begin{array}{c} f111 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline \\ & & & & \\ & & & \\ & & & & \\ & & & &$	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \end{array}$	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT & 10\% & 90\% & RT_{\rm SUCC} \\ 15 \ 1.4e6 & 1.1e6 & 1.8e6 & 1.4e6 \\ 0 & 66e-1 & 46e-1 & 85e-1 & 2.2e6 \\ . & . & . & . \\ . & . & . & . \\ f113 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT & 10\% & 90\% & RT_{\rm SUCC} \\ 15 \ 1.2e3 & 8.3e2 & 1.5e3 & 1.2e3 \\ 15 \ 6.6e5 & 4.6e5 & 8.6e5 & 6.6e5 \\ 0 & 31e-2 & 17e-2 & 57e-2 & 2.8e6 \\ . & . & . & . \\ . & . & . & . \\ . & . &$	$ \begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ & & & & & & \\ & & & & & & \\ & & & & $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-8 \\ $	f111 in 5-D, N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ} 15 1.4e6 1.4e6 85e-1 2.2e6 0 66e-1 46e-1 85e-1 2.2e6 113 in 5-D, N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ} f113 in 5-D, N=15, mFE=5.00 e6 f115 in 5-D, N=15, mFE=5.00 e6 f115 in 5-D, N=15, mFE=5.00 e6 f115 in 5-D, N=15, mFE=5.00 e6	$ \begin{array}{c} f111 \ \mbox{in 20-D}, \ N=15, \ mFE=2.00e7 \\ \# \ \ ERT \ \ 10\% \ \ 90\% \ \ RT_{succ} \\ \hline 0 \ \ 94e+2 \ \ 73e+2 \ \ 12e+3 \ \ \ 6.3e6 \\ \hline \\ \hline \\ f113 \ \ \ in \ \ 20-D, \ \ N=15, \ \ mFE=2.00e7 \\ \# \ \ ERT \ \ \ 10\% \ \ 90\% \ \ \ RT_{succ} \\ \hline \\ \hline 0 \ \ 95e+0 \ \ 79e+0 \ \ 11e+1 \ \ 8.9e6 \\ \hline \\ \hline \\ \hline \\ f115 \ \ \ in \ \ 20-D, \ \ N=15, \ \ mFE=2.00e7 \\ \hline \\ \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \begin{array}{c} le - 8 \\ \Delta f \\ 10 \\ 1 \\ $	f111 in 5-D, N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ} 15 1.4e6 1.4e6 8.8e6 1.4e6 0 66e-1 46e-1 8.5e-1 2.2e6 f113 in 5-D, N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ} 15 6.6e5 4.6e5 8.6e5 6.6e5 0 31e-2 17e-2 57e-2 2.8e6 15 6.6e5 1.6e5 8.6e5 6.6e5 0 31e-2 17e-2 57e-2 2.8e6 f115 in 5-D, N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ}	<pre>f111 in 20-D, N=15, mFE=2.00e7 # ERT 10% 90% RT_{BUCC} 0 94e+2 73e+2 12e+3 6.3e6</pre>	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1e-1 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \end{array}$	$ \begin{array}{c} f111 \mbox{ in } 5-D, \mbox{ N=15}, \mbox{ mFE=5.00 e6} \\ \# \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	$ \begin{array}{c} f_{111} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3 \text{ e6} \\ \hline \\ & & & & & & & \\ \hline \\ f_{113} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9 \text{ e6} \\ \hline \\ & & & & & & \\ \hline \\ f_{115} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ 0 & 11e+1 & 77e+0 & 12e+1 & 1.3 \text{ e7} \\ \hline \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ \end{array}$	$ \begin{array}{c} f111 \mbox{ in } 5-D, \ N=15, \ mFE=5.00 \mbox{ ef} \\ \# \ ERT \ 10\% \ 90\% \ RT_{\rm succ} \\ 15 \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 0 \ 66e \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 15 \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 16e \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 16e \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 15e \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 113 \mbox{ in } 5-D, \ N=15, \ mFE=5.00 \mbox{ ef} \\ 15 \ 1.2 \mbox{ ef} \ 3.3 \mbox{ ef} \ 1.2 \mbox{ ef} \ 1.2 \mbox{ ef} \\ 15 \ 1.2 \mbox{ ef} \ 3.3 \mbox{ ef} \ 1.5 \mbox{ ef} \ 1.2 \mbox{ ef} \ 1.4 \mbox{ ef} \\ 15 \ 1.2 \mbox{ ef} \ 3.3 \mbox{ ef} \ 1.5 \mbox{ ef} \ 1.2 \m$	$ \begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline \\ & & & & & & \\ \hline \\ f113 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ 0 & 95e+0 & 79e+0 & 11e+1 & 8.9e6 \\ \hline \\ & & & & & \\ \hline \\ f115 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ f115 \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ \hline 0 & 11e+1 & 77e+0 & 12e+1 & 1.3e7 \\ \hline \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\$	$ \begin{array}{c} \textbf{f111 in 5-D, N=15, mFE=5.00e6} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ 15 \ 1.4e6 \ 1.1e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$ \begin{array}{c} f111 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline \\ \hline \\ 113 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ \hline 0 \ 95e+0 \ 79e+0 \ 11e+1 \ 8.9e6 \\ \hline \\ \hline \\ \hline \\ 115 \ \text{in 20-D, N=15, mFE=2.00e7} \\ \# \ \text{ERT} \ 10\% \ 90\% \ \text{RT}_{\text{succ}} \\ \hline \hline \\ 0 \ 71e+1 \ 77e+0 \ 12e+1 \ 1.3e7 \\ \hline \\ \hline \\ \hline \\ \hline \\ \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \underline{\Delta f} \\ 1 \\ 1e-3 \\ 1e-8 $	$ \begin{array}{c} f111 \mbox{in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT & 10\% & 90\% & RT_{succ} \\ 15 \ 1.4 e6 & 1.1 e6 & 1.8 e6 & 1.4 e6 \\ 0 & 66e-1 & 46e-1 & 85e-1 & 2.2 e6 \\ . & . & . & . & . \\ f113 \mbox{in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT & 10\% & 90\% & RT_{succ} \\ 15 \ 1.2 e3 & 8.3 e2 & 1.5 e3 & 1.2 e3 \\ 15 \ 6.6 e5 & 4.6 e5 & 8.6 e5 & 6.6 e5 \\ 0 & 31e-2 & 17e-2 & 57e-2 & 2.8 e6 \\ . & . & . & . \\ f115 \mbox{in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT & 10\% & 90\% & RT_{succ} \\ 15 \ 1.4 e3 & 9.8 e2 & 1.7 e3 & 1.4 e3 \\ 15 \ 1.4 e3 & 9.8 e2 & 1.7 e3 & 1.4 e3 \\ 15 \ 4.4 e5 & 3.3 e5 & 5.4 e5 & 4.4 e5 \\ 0 \ 34e-2 \ 16e-2 \ 53e-2 & 2.2 e6 \\ . & . & . & . \\ . & . & . & . \\ . & . &$	$ \begin{array}{c} f_{111} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline \\ f_{113} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9e6 \\ \hline \\ f_{115} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 11e+1 & 77e+0 & 12e+1 & 1.3e7 \\ \hline \\ \hline \\ f_{117} \text{ in } 20\text{-D}, \text{ N=15}, \text{ mFE=2.00e7} \\ \hline \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \Delta f \\ \hline 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline \Delta f \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ \Delta f \end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ \end{array}$	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.4e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e-1 \ 46e-1 \ 85e-1 \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$ \begin{array}{c} f111 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6\\ \hline \\ 113 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline 0 \ 95e+0 \ 79e+0 \ 11e+1 \ 8.9e6\\ \hline \\ 115 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \hline 1115 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \\ 1117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \\ 1117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1e-8 \\ \Delta f \\ 10 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 1e-8 \\ \Delta f \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-1$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} f111 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6\\ \hline \\ \hline \\ 113 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline 0 \ 95e+0 \ 79e+0 \ 11e+1 \ 8.9e6\\ \hline \\ \hline \\ \hline \\ 115 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \hline \\ 0 \ 11e+1 \ 77e+0 \ 12e+1 \ 1.3e7\\ \hline \\ \hline \\ \hline \\ \hline \\ 117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \hline \\ \hline \\ 117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ}\\ \hline \\ \hline \\ \hline \\ 117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ 117 \ in \ 20\text{-D}, \ N=15, \ mFE=2.00e7\\ \hline \\ \hline$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} {\rm le-8}\\ {\rm A}f\\ 10\\ 1\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm A}f\\ 10\\ 1\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm A}f\\ 10\\ 1\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm A}f\\ 10\\ 1\\ {\rm le-3}\\ 1\\ $	$ \begin{array}{c} f111 \mbox{in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{\rm SHCC} \\ 15 \ 1.4e6 \ 1.1e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$ \begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3e6 \\ \hline \\ f113 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9e6 \\ \hline \\ f115 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 11e+1 & 77e+0 & 12e+1 & 1.3e7 \\ \hline \\ f117 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 14e+1 & 77e+2 & 66e+2 & 1.6e7 \\ \hline \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} {\rm le-8} \\ {\rm af} \\ {\rm fl} \\ {\rm fl} \\ {\rm le-3} \\ {\rm le-4} \\ {\rm le-1} \\ {\rm le-3} \\$	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.1e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e-1 \ 46e-1 \ 85e-1 \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$ \begin{array}{c} f111 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3 \text{ e6} \\ \hline 0 & 94e+2 & 73e+2 & 12e+3 & 6.3 \text{ e6} \\ \hline \\ f113 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9 \text{ e6} \\ \hline \\ \hline \\ f115 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 11e+1 & 77e+0 & 12e+1 & 1.3 \text{ e7} \\ \hline \\ \hline \\ f117 \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 44e+2 & 37e+2 & 66e+2 & 1.6 \text{ e7} \\ \hline \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-8} \\$	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.4e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} {\rm le-8}\\ {\rm le-8}\\ {\rm 10}\\ {\rm 1}\\ {\rm le-1}\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm le-8}\\ {\rm le-8}\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm le-8}\\ {\rm le-8}\\ {\rm le-1}\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm le-8}\\ {\rm le-1}\\ {\rm le-3}\\ {\rm le-5}\\ {\rm le-8}\\ {\rm l$	$ \begin{array}{c} f111 \mbox{in 5-D, N=15, mFE=5.00e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.1e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$		$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} {\rm le}{\rm -8} \\ {\rm \Delta}f \\ {\rm 10} \\ {\rm 1} \\ {\rm le}{\rm -3} \\ {\rm le}{\rm -5} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm -5} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm -1} \\ {\rm le}{\rm -3} \\ {\rm le}{\rm -5} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm -1} \\ {\rm le}{\rm -3} \\ {\rm le}{\rm -5} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm -1} \\ {\rm le}{\rm -3} \\ {\rm le}{\rm -5} \\ {\rm le}{\rm -8} \\ {\rm le}{\rm le}{\rm -8} \\ {\rm le}{\rm le}{\rm le}{\rm -8} \\ {\rm le}{\rm l}{\rm le}{\rm le}{\rm le}{\rm le}{\rm l}{\rm le}{\rm le}{\rm le}{\rm le}{\rm l}{\rm le}{\rm le}{\rm l}{\rm le}{\rm l}{\rm le}{\rm l}{\rm l}{\rm le}{\rm l}{\rm l}{\rm l}{\rm l}{\rm l}{\rm l}{$	$ \begin{array}{c} f_{111} \mbox{in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4 e6 \ 1.1 e6 \ 1.8 e6 \ 1.4 e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2 e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$\begin{array}{c} f_{111} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 94e+2 & 78e+2 & 12e+3 & 6.3e6 \\ \hline 0 & 94e+2 & 78e+2 & 12e+3 & 6.3e6 \\ \hline \\ & & & & & & & & & & \\ f_{113} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 95e+0 & 79e+0 & 11e+1 & 8.9e6 \\ \hline \\ & & & & & & & & \\ f_{115} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 11e+1 & 77e+0 & 12e+1 & 1.3e7 \\ \hline \\ & & & & & & & & \\ f_{117} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline 0 & 44e+2 & 37e+2 & 66e+2 & 1.6e7 \\ \hline \\ & & & & & & & \\ f_{119} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline f_{119} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline f_{119} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline f_{119} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \# \text{ ERT } 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ N=15} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{ mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D}, \text{mFE=2.00e7} \\ \hline f_{110} \text{ in } 20\text{-D} \\ \hline f_{$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\$	$ \begin{array}{c} f111 \mbox{in 5-D}, N=15, \mbox{mFE}=5.00 {\rm e6} \\ \# \ {\rm ERT} & 10\% & 90\% & {\rm RT}_{\rm succ} \\ 15 \mbox{1.4e6} & 1.1e6 & 1.8e6 & 1.4e6 \\ 0 & 66e-1 & 46e-1 & 85e-1 & 2.2e6 \\ . & . & . & . & . \\ . & . & . & . & .$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} f111 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline \\ \hline \\ 113 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ 0 \ 95e+0 \ 79e+0 \ 11e+1 \ 8.9e6 \\ \hline \\ \hline \\ \hline \\ 115 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ 1117 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ 1117 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ 1117 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ 1117 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ 116 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ 116 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ 116 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ \hline \\ 116 \ in \ 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline \\ \hline \\ \hline \\ 15 \ 4.9e6 \ 3.7e6 \ 6.1e6 \ 4.9e6 \\ \hline \\ 0 \ 84e-1 \ 68e-1 \ 96e-1 \ 8.9e6 \\ \hline \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\$	$ \begin{array}{c} f111 \mbox{ in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4 e6 \ 1.1 e6 \ 1.8 e6 \ 1.4 e6 \\ 0 \ 66e-1 \ 46e-1 \ 85e-1 \ 2.2 e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{fl} \\ \mathrm{fl} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-3} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-8} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-1} \\ \mathrm{le}{-3} \\ \mathrm{le}{-5} \\ \mathrm{le}{-8} \\ \mathrm{le}{-$	$ \begin{array}{c} f111 \mbox{in 5-D, N=15, mFE=5.00 e6} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ 15 \ 1.4e6 \ 1.1e6 \ 1.8e6 \ 1.4e6 \\ 0 \ 66e^{-1} \ 46e^{-1} \ 85e^{-1} \ 2.2e6 \\ . \ . \ . \ . \ . \ . \ . \ . \ . \ .$	$\begin{array}{c} f111 \mbox{ in 20-D, N=15, mFE=2.00e7} \\ \# \mbox{ ERT } 10\% \ 90\% \ RT_{succ} \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline 0 \ 94e+2 \ 73e+2 \ 12e+3 \ 6.3e6 \\ \hline 1113 \mbox{ in 20-D, N=15, mFE=2.00e7} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline 0 \ 95e+0 \ 79e+0 \ 11e+1 \ 8.9e6 \\ \hline 0 \ 11e+1 \ 77e+0 \ 12e+1 \ 1.3e7 \\ \hline 0 \ 11e+1 \ 77e+0 \ 12e+1 \ 1.3e7 \\ \hline 0 \ 11e+1 \ 77e+0 \ 12e+1 \ 1.3e7 \\ \hline 0 \ 14e+2 \ 37e+2 \ 66e+2 \ 1.6e7 \\ \hline 0 \ 44e+2 \ 37e+2 \ 66e+2 \ 1.6e7 \\ \hline 1119 \ mbox{ in 20-D, N=15, mFE=2.00e7} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline 1119 \ mbox{ in 20-D, N=15, mFE=2.00e7} \\ \# \ ERT \ 10\% \ 90\% \ RT_{succ} \\ \hline 0 \ 44e+2 \ 37e+2 \ 66e+2 \ 1.6e7 \\ \hline 15 \ 4.9e6 \ 3.7e6 \ 6.1e6 \ 4.9e6 \\ \hline 0 \ 84e-1 \ 68e-1 \ 96e-1 \ 8.9e6 \\ \hline \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Table 1: Shown are, for functions $f_{101}-f_{120}$ and for a given target difference to the optimal function value Δf : the number of successful trials (#); the expected running time to surpass $f_{opt} + \Delta f$ (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (\mathbf{RT}_{succ}). If $f_{opt} + \Delta f$ was never reached, figures in *italics* denote the best achieved Δf -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.



Figure 2: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left subplots) or versus Δf (right subplots). The thick red line represents the best achieved results. Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension D, to fall below $f_{opt} + \Delta f$ with $\Delta f = 10^k$, where k is the first value in the legend. Right subplots: ECDF of the best achieved Δf divided by 10^k (upper left lines in continuation of the left subplot), and best achieved Δf divided by 10^{-8} for running times of D, 10D, 100D... function evaluations (from right to left cycling blackcyan-magenta). Top row: all results from all functions; second row: moderate noise functions; third row: severe noise functions; fourth row: severe noise and highly-multimodal functions. The legends indicate the number of functions that were solved in at least one trial. FEvals denotes number of function evaluations, Dand DIM denote search space dimension, and Δf and Df denote the difference to the optimal function value.

	f121 in 5-D, N=15, mFE=5.00e6	f121 in 20-D, N=15, mFE=2.00e7	f122 in 5-D, N=15, mFE=5.00e6	f_{122} in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	Δf # ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}
10	15 2.1e1 1.5e1 2.7e1 2.1e1	14 6.4e6 4.4e6 8.3e6 6.2e6	10 15 2.0e1 1.4e1 2.6e1 2.0e1	15 8.6e3 4.8e3 1.3e4 8.6e3
1	15 5.9e3 4.0e3 7.8e3 5.9e3	0 82e-1 66e-1 10e+0 1.0e7	1 15 1.8e5 1.4e5 2.3e5 1.8e5	0 49e-1 44e-1 56e-1 1.0e7
$1\mathrm{e}-1$	9 5.6e6 4.3e6 8.7e6 3.4e6		1e-1 0 $46e-2$ $31e-2$ $56e-2$ $2.2e6$	
$1\mathrm{e}-3$	0 87e-3 36e-3 14e-2 2.0e6		1e-3	
$1\mathrm{e}-5$			1e-5	
$1\mathrm{e}-8$			1e-8	
	f123 in 5-D, N=15, mFE=5.00e6	f123 in 20-D, N=15, mFE=2.00e7	f124 in 5-D, N=15, mFE=5.00e6	f124 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{succ}$	# ERT 10% 90% RT _{succ}
10	15 1.1e1 8.1e0 1.4e1 1.1e1	15 7.9e3 4.8e3 1.0e4 7.9e3	10 15 1.9e1 1.4e1 2.3e1 1.9e1	15 8.9e3 3.7e3 1.5e4 8.9e3
1	15 2.4e5 2.0e5 2.8e5 2.4e5	0 53e-1 48e-1 57e-1 1.0e7	1 15 1.9e5 1.2e5 2.7e5 1.9e5	0 51e-1 48e-1 57e-1 1.1e7
1e-1	0 49e-2 30e-2 58e-2 2.2e6		1e-1 0 46e-2 25e-2 61e-2 2.5e6	
1e-3			1e-3	
1e-5			1e-5	
1e-8			1e-8	
	f125 in 5-D, N=15, mFE=5.00e6	f125 in 20-D, N=15, mFE=2.00e7	f126 in 5-D, N=15, mFE=5.00e6	f126 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{SUCC}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{SUCC}$	# ERT 10% 90% RT _{succ}
10	15 1.1e0 1.0e0 1.3e0 1.1e0	15 1.0e0 1.0e0 1.0e0 1.0e0	10 15 1.1e0 1.0e0 1.3e0 1.1e0	15 1.1e0 1.0e0 1.1e0 1.1e0
1	15 6.0e1 3.1e1 8.3e1 6.0e1	15 5.9e5 4.4e5 7.9e5 5.9e5	1 15 4.3e1 2.8e1 5.4e1 4.3e1	15 3.2e5 2.0e5 4.3e5 3.2e5
1e-1	15 1.5e5 1.1e5 2.0e5 1.5e5	0 80e-2 70e-2 85e-2 7.9e6	1e-1 15 1.2e5 9.6e4 1.5e5 1.2e5	0 76e-2 72e-2 81e-2 8.9e6
1e-3	0 36e-3 21e-3 44e-3 3.2e6		1e-3 0 34e-3 24e-3 51e-3 1.4e6	
1e-5			1e-5	
$1\mathrm{e}-8$			1e-8	
	f127 in 5-D, N=15, mFE=5,00e6	f127 in 20-D, N=15, mFE=2.00e7	f_{128} in 5-D, N=15, mFE=5.00e6	f128 in 20-D, N=15, mFE=2.00 e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{SUCC}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{SUCC}$	# ERT 10% 90% RT _{SUCC}
10	15 1.0e0 1.0e0 1.0e0 1.0e0	15 1.3e0 1.1e0 1.4e0 1.3e0	10 15 2.0e2 1.4e2 2.5e2 2.0e2	$0 \ 24e+0 \ 15e+0 \ 31e+0 \ 1.0e7$
1	15 4.7e1 3.5e1 6.0e1 4.7e1	15 5.2e5 3.9e5 6.8e5 5.2e5	1 15 1.7e4 1.4e4 2.1e4 1.7e4	
1e-1	15 1.2e5 8.6e4 1.6e5 1.2e5	0 79e-2 67e-2 83e-2 7.9e6	1e-1 15 3.2e5 2.0e5 4.3e5 3.2e5	
1e-3	0 33e-3 15e-3 44e-3 2.0e6		1e-3 1 7.4e7 3.7e7 >7e7 4.1e6	
1e-5			1e-5 0 $10e-3$ $11e-4$ $22e-3$ $2.0e6$	
1e-8			1e-8	
	f129 in 5-D, N=15, mFE=5,00e6	f129 in 20-D, N=15, mFE=2.00e7	f_{130} in 5-D, N=15, mFE=5.00e6	f130 in 20-D, N=15, mFE=2.00 e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{SUCC}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{\text{SUCC}}$	# ERT 10% 90% RT _{succ}
10	15 1.8e2 1.4e2 2.4e2 1.8e2	0 24e+0 23e+0 29e+0 7.9e6	10 15 1.7e2 1.3e2 2.2e2 1.7e2	$0 \ 25e+0 \ 18e+0 \ 29e+0 \ 1.3e7$
1	15 1.4e4 1.1e4 1.7e4 1.4e4		1 15 2.5e4 1.7e4 3.2e4 2.5e4	
$1\mathrm{e}-1$	15 3.4e5 2.7e5 4.2e5 3.4e5		1e-1 15 3.3e5 2.4e5 4.0e5 3.3e5	
1e-3	1 7.4e7 3.7e7 >7e7 5.0e6		1e-3 1 7.4e7 2.5e7 >7e7 5.0e6	
1e-5	0 13e-3 12e-4 31e-3 2.5e6		1e-5 0 $42e-4$ $16e-4$ $15e-3$ 2.5e6	
$1\mathrm{e}-8$			1e-8	
	•	•	-	1

Table 2: Shown are, for functions f_{121} - f_{130} and for a given target difference to the optimal function value Δf : the number of successful trials (#); the expected running time to surpass $f_{opt} + \Delta f$ (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (\mathbf{RT}_{succ}). If $f_{opt} + \Delta f$ was never reached, figures in *italics* denote the best achieved Δf -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.