Benchmarking the (1+1)-ES with One-Fifth Success rule on the BBOB-2009 Noisy Testbed

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ABSTRACT

The (1+1)-ES with one-fifth success rule is one of the first and simplest stochastic algorithm proposed for optimization on a continuous search space in a black-box scenario. In this paper, we benchmark an independent-restart (1+1)-ES with one-fifth success rule on the BBOB-2009 noisy testbed. The maximum number of function evaluations used equals 10^6 times the dimension of the search space. The algorithm could only solve 3 functions with moderate noise in 5-D and 2 functions in 20-D.

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization—global optimization, unconstrained optimization; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

Algorithms

Keywords

Benchmarking, Black-box optimization, Evolutionary computation

1. INTRODUCTION

The (1+1)-ES with one-fifth success rule is one of the earliest and simplest adaptive stochastic search algorithm [8, 7, 3]. This paper complements [1] where an independentrestart implementation of the (1+1)-ES with one-fifth success rule is benchmarked on the BBOB-2009 noise-free testbed. Indeed, we test exactly the same algorithm, using the same settings on the BBOB-2009 noisy testbed. For the description of the algorithm and the settings we refer to [1].

2. RESULTS AND DISCUSSION

Results from experiments according to [5] on the benchmark functions given in [4, 6] are presented in Figures 1 and 2 and in Tables 1 and 2.

We observe that globally the algorithm performs poorly. In 5-D, only f_{101} , f_{102} , f_{103} are solved and in 20-D only f_{101} and f_{102} are solved. The functions solved belong to the class of functions with moderate noise.

Acknowledgments

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Figure 1: Expected Running Time (ERT, •) to reach $f_{opt} + \Delta f$ and median number of function evaluations of successful trials (+), shown for $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$ (the exponent is given in the legend of f_{101} and f_{130}) versus dimension in log-log presentation. The ERT(Δf) equals to $\#FEs(\Delta f)$ divided by the number of successful trials, where a trial is successful if $f_{opt} + \Delta f$ was surpassed during the trial. The $\#FEs(\Delta f)$ are the total number of function evaluations while $f_{opt} + \Delta f$ was not surpassed during the trial from all respective trials (successful and unsuccessful), and f_{opt} denotes the optimal function value. Crosses (×) indicate the total number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

	f101 in 5-D, N=15, mFE=438	f101 in 20-D, N=15, mFE=2971	f102 in 5-D, N=15, mFE=886 f	102 in 20-D , N=15, mFE=2.00e7
_	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{\text{succ}}$	# ERT 10% 90% RT _{succ}	Δf # ERT 10% 90% RT _{succ} #	ERT 10% 90% RT _{succ}
	10 15 3.2e1 2.7e1 3.8e1 3.2e1 1 15 6.7e1 5.9e1 7.4e1 6.7e1	$15 \ 2.9e2 \ 2.4e2 \ 3.5e2 \ 2.9e2 \ 15 \ 4.3e2 \ 3.7e2 \ 4.9e2 \ 4.3e2$	1 15 7 6e1 6 9e1 8 2e1 7 6e1 15	0.1e2 5.0e2 7.2e2 0.1e2 1.6e3 1.2e3 2.0e3 1.6e3
10	e-1 15 1.1e2 9.9e1 1.2e2 1.1e2	15 5.7e2 5.2e2 6.3e2 5.7e2	1e-1 15 1.1e2 1.0e2 1.2e2 1.1e2 15	3.2e3 2.4e3 4.0e3 3.2e3
1	e-3 15 1.9e2 1.8e2 2.0e2 1.9e2	$15 \ 8.4\mathrm{e}2 \ 7.9\mathrm{e}2 \ 9.0\mathrm{e}2 \ 8.4\mathrm{e}2$	1e-3 15 2.0e2 1.9e2 2.0e2 2.0e2 15	1.8e4 1.4e4 2.3e4 1.8e4
10	e-5 15 2.6e2 2.5e2 2.7e2 2.6e2	15 1.1e3 1.1e3 1.2e3 1.1e3	1e-5 15 2.8e2 2.7e2 2.9e2 2.8e2 15	3.4e5 2.4e5 4.4e5 3.4e5
10	5-8 15 3.8e2 3.7e2 3.9e2 3.8e2	15 1.6e3 1.5e3 1.8e3 1.6e3	1e-8 15 4.3e2 4.0e2 4.8e2 4.3e2 9	2.3e7 1.7e7 3.3e7 1.3e7
Δf	# ERT 10% 90% RTsucc	# ERT 10% 90% RTsucc	$\Delta f = \frac{104 \text{ in 5-D}}{4 \text{ ERT}}$ N=15, mFE=5.00e6	# ERT 10% 90% RTsucc
10	15 3.3e1 2.5e1 4.1e1 3.3e1	15 2.2e2 2.1e2 2.3e2 2.2e2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	15 1.1e6 8.0e5 1.3e6 1.1e6
1	15 6.8e1 6.1e1 7.5e1 6.8e1	15 4.6e2 3.9e2 5.3e2 4.6e2	1 15 3.3e3 2.3e3 4.4e3 3.3e3	6 3.8e7 2.5e7 6.5e7 1.5e7
1e - 1	15 1.1e2 9.9e1 1.1e2 1.1e2	15 1.0e3 8.5e2 1.3e3 1.0e3	1e-1 15 1.5e4 1.1e4 2.0e4 1.5e4	2 1.3e8 6.6e7 > 3e8 1.2e7
1e - 3 1e - 5	$15 \ 1.8e4 \ 9.3e3 \ 2.9e4 \ 1.8e4$	0 42e-5 32e-5 74e-5 7.9e6	1e-5 14 2.0e6 1.5e6 2.6e6 2.0e6	0 12e-1 57e-5 55e-1 7.5e0
$1\mathrm{e}-8$	13 2.6e6 1.9e6 3.3e6 2.4e6		1e-8 0 $25e-8$ $15e-9$ $73e-7$ $1.8e6$	
	f105 in 5-D, N=15, mFE=5.00 e6	f105 in 20-D, N=15, mFE=2.00 e7	f106 in 5-D, N=15, mFE=5.00e6	f106 in 20-D, N=15, mFE=2.00e7
$\frac{\Delta f}{10}$	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{\text{succ}}$	# ERT 10% 90% RT _{succ}
1	15 2.4e3 1.9e3 2.9e3 2.4e3	0 13e+0 37e-1 15e+0 1.1e7	10 13 1.3e2 1.1e2 1.4e2 1.3e2 1 15 3.5e3 2.4e3 4.6e3 3.5e3	$15 \ 5.264 \ 4.064 \ 1.465 \ 5.264$ $15 \ 4.666 \ 3.566 \ 5.866 \ 4.666$
$1\mathrm{e}-1$	15 6.9e3 5.0e3 8.9e3 6.9e3		1e-1 15 1.8e4 1.3e4 2.4e4 1.8e4	0 42e-2 13e-2 62e-2 1.0e7
1e - 3	15 1.7e5 1.2e5 2.2e5 1.7e5		1e-3 15 6.9e5 4.6e5 9.4e5 6.9e5	
1e - 5 1e - 8	14 1.9e6 1.4e6 2.4e6 1.8e6 0 $42e-8 13e-8 38e-7$ 2.8e6		1e-5 0 $10e-5$ $35e-6$ $28e-5$ $3.2e61e-8$	
0	f_{107} in 5-D, N=15, mFE=5.00e6	f107 in 20-D, N=15, mFE=2.00e7	f108 in 5-D, N=15, mFE=5.00e6	f108 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{succ}$	# ERT 10% 90% RT _{succ}
10	15 1.2e3 8.3e2 1.6e3 1.2e3	$0 34e+0 28e+0 48e+0 \qquad 1.0e7$	10 15 2.1e3 1.4e3 2.8e3 2.1e3	$0 41e+0 33e+0 \overline{49e+0} \qquad 1.0 \text{ e7}$
1e – 1	15 1.3e4 1.1e4 1.0e4 1.3e4 15 2.9e5 1.9e5 4.0e5 2.9e5		1 15 1.0e5 1.1e5 2.0e5 1.0e5 1e-1 5 1.2e7 7 7e6 2.3e7 3 3e6	
1e - 3	1 7.1e7 3.3e7 >7e7 5.9e5		1e-3 0 $12e-2$ $41e-3$ $24e-2$ $2.2e6$	
$1\mathrm{e}-5$	0 50e-4 13e-4 16e-3 2.8e6		1e-5	
1e-8	· · · · · · · ·	· · · · · · · · ·	1e-8	
Δf	$f_{109 \text{ in } 5-D}$, N=15, mFE=5.00e6 # EBT 10% 90% BT	$f_{109 \text{ in } 20\text{-}D}$, N=15, mFE=2.00e7 # EBT 10% 90% BT_	f_{110} in 5-D, N=15, mFE=5.00e6 # EBT 10% 90% BT	f_{110} in 20-D, N=15, mFE=2.00e7 # EBT 10% 90% BT_{mean}
10	$\frac{\pi}{15}$ 3.0e1 2.4e1 3.6e1 3.0e1	$\frac{\pi}{15}$ 1.9e3 1.4e3 2.4e3 1.9e3	10 15 2.0e4 1.4e4 2.5e4 2.0e4	0 11e+3 77e+2 16e+3 7.1e6
1	15 3.1e2 2.3e2 3.8e2 3.1e2	15 2.4e6 1.6e6 3.3e6 2.4e6	1 15 1.1e6 7.8e5 1.4e6 1.1e6	
1e - 1	15 2.9e3 2.1e3 3.7e3 2.9e3	0 72e-2 58e-2 82e-2 1.4e7	1e-1 0 $29e-2$ $15e-2$ $49e-2$ $3.2e6$	
1e - 3 1e - 5	$(8.1eb \ 5.0eb \ 1.3e7 \ 3.0eb \ 0 \ 13e-4 \ 23e-5 \ 22e-4 \ 3.2e6 \ 3.2e6$		1e-3	
1e-8			1e-8	
	f111 in 5-D, N=15, mFE=5.00e6	f111 in 20-D, N=15, mFE=2.00e7	f112 in 5-D, N=15, mFE=5.00e6	f112 in 20-D, N=15, mFE=2.00e7
Δf	# EBT 10% 90% BT _{auga}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ERT} 10\% 90\% \text{RT}_{\text{succ}}$	# ERT 10% 90% RT _{succ}
10	17 0 0 F 0 1 F 1 1 0 0 0 F			
10	$\begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \end{array}$	0 15e+3 11e+3 20e+3 1.1e7	10 15 2.5e2 1.9e2 3.1e2 2.5e2 1 15 7.6e3 5.3e3 1.0e4 7.6e3	2 1.4e8 6.8e7 > 3e8 1.4e7 0 15e+0 87e-1 17e+0 7.9e6
$10 \\ 1 \\ 1e-1$	$ \begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ \end{array} $	$ \begin{array}{c} 0 & 15e+3 & 11e+3 & 20e+3 & 1.1e7 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots & \vdots & \vdots$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 1 1e-1 1e-3	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 1 1e-1 1e-3 1e-5 1a	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 1 1e-1 1e-3 1e-5 1e-8	15 8.8e5 6.1e5 1.1e6 8.8e5 0 45e-1 22e-1 66e-1 2.8e6 	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \frac{10}{1} $ $ \frac{1}{1e-1} $ $ \frac{1e-3}{1e-5} $ $ \frac{1e-5}{1e-8} $ $ \Delta f $	15 8.8e5 6.1e5 1.1e6 8.8e5 0 45e-1 22e-1 66e-1 2.8e6 <td>0 15e+3 11e+3 20e+3 1.1e7 </td> <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td>	0 15e+3 11e+3 20e+3 1.1e7 	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ -3 \\ 1 \\ -5 \\ 1 \\ -5 \\ 1 \\ -8 \\ \hline \begin{array}{c} \Delta f \\ 1 \\ 1 \\ 1 \\ 1 \\ -3 \\ 1 \\ -3 \end{array}$	$\begin{array}{c} 1 \\ 5 \\ 8.8e5 \\ 6.1e5 \\ 1.1e6 \\ 8.8e5 \\ 0 \\ 45e-1 \\ 22e-1 \\ 66e-1 \\ 2.8e6 \\ .$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ \end{array}$	15 8.8e5 6.1e5 1.1e6 8.8e5 0 $45e-1$ $22e-1$ $66e-1$ 2.8e6 f113 in 5-D, N=15, mFE=5.00e6 . . # ERT 10% 90% RTsucc 15 6.1e4 1.4e3 2.2e3 1.8e3 15 6.1e4 1.2e6 2.7e6 1.4e6 0 $23e-3$ $96e-4$ 11e-2 2.2e6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline \Delta f \\ 10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \end{array}$	$\begin{array}{c} \textbf{15} \hspace{0.5mm} 8.8e5 \hspace{0.5mm} 6.1e5 \hspace{0.5mm} 1.1e6 \hspace{0.5mm} 8.8e5 \\ 0 \hspace{0.5mm} 45e^{-1} \hspace{0.5mm} 22e^{-1} \hspace{0.5mm} 66e^{-1} \hspace{0.5mm} 2.8e5 \\ \hline \textbf{113} \hspace{0.5mm} \textbf{in} \hspace{0.5mm} 5\text{-}\textbf{D}, \hspace{0.5mm} \textbf{N} = 15, \hspace{0.5mm} \textbf{mFE} = 5.00 \hspace{0.5mm} e6 \hspace{0.5mm} \\ \hline \textbf{in} \hspace{0.5mm} \textbf$	$ \begin{array}{c} \begin{array}{c} & 0 & 15e+3 & 11e+3 & 20e+3 & 1.1e7 \\ \hline & & & & & & \\ & & & & & & \\ & & & &$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \frac{1}{10} \frac{1}{1} \frac{1}{1e^{-1}} \frac{1}{1e^{-3}} \frac{1}{1e^{-5}} \frac{1}{1e^{-3}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-8}} \frac{1}{1e^{-5}} \frac{1}{1e^{-$	$\begin{array}{c} \textbf{15} \hspace{0.5mm} 8.8e5 \hspace{0.5mm} 6.1e5 \hspace{0.5mm} 1.1e6 \hspace{0.5mm} 8.8e5 \hspace{0.5mm} \\ 0 \hspace{0.5mm} 45e^{-1} \hspace{0.5mm} 22e^{-1} \hspace{0.5mm} 66e^{-1} \hspace{0.5mm} 2.8e5 \hspace{0.5mm} \\ 0 \hspace{0.5mm} 45e^{-1} \hspace{0.5mm} 22e^{-1} \hspace{0.5mm} 66e^{-1} \hspace{0.5mm} 2.8e5 \hspace{0.5mm} \\ \hline \end{array} \\ \begin{array}{c} \textbf{1113} \hspace{0.5mm} \textbf{in} \hspace{0.5mm} \textbf{5-D}, \hspace{0.5mm} \textbf{N=15}, \hspace{0.5mm} \textbf{MFE}{=}5.00\hspace{0.5mm} 66 \hspace{0.5mm} \\ \hline \end{array} \\ \begin{array}{c} \textbf{\#} \hspace{0.5mm} \textbf{ERT} \hspace{0.5mm} 10\% \hspace{0.5mm} 90\% \hspace{0.5mm} \textbf{RTsucc} \hspace{0.5mm} \\ \hline \textbf{5} \hspace{0.5mm} 1.8e3 \hspace{0.5mm} 1.4e3 \hspace{0.5mm} 2.2e3 \hspace{0.5mm} 1.8e3 \hspace{0.5mm} \\ \hline \textbf{13} \hspace{0.5mm} 1.9e\hspace{0.5mm} 61.2e6 \hspace{0.5mm} 2.7e6 \hspace{0.5mm} 1.4e6 \hspace{0.5mm} \\ \hline \textbf{0} \hspace{0.5mm} 23e^{-3} \hspace{0.5mm} 96e^{-4} \hspace{0.5mm} 11e^{-2} \hspace{0.5mm} 2.2e6 \hspace{0.5mm} \\ \hline \end{array} \\ \begin{array}{c} \textbf{.} \\ \textbf{.} \end{array} \\ \begin{array}{c} \textbf{1115} \hspace{0.5mm} \textbf{in} \hspace{0.5mm} \textbf{5-D}, \hspace{0.5mm} \textbf{N=15}, \hspace{0.5mm} \textbf{MFE}{=} 5.00\hspace{0.5mm} e6 \hspace{0.5mm} \end{array} \end{array}$	$ \begin{array}{c} \begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ &$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} -10 \\ 1 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline \Delta f \\ 10 \\ 1e-1 \\ 1e-3 \\ 1e-5 \\ 1e-8 \\ \hline \Delta f \\ 10 \\ \hline \end{array}$	$\begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ & & & & & & \\ & & & & & & \\ & & & & $	$ \begin{array}{c} \begin{array}{c} & & & & & \\ 0 & 15e+3 & 11e+3 & 20e+3 & 1.1e7 \\ & & & & & & \\ \end{array} \\ \hline \\ f113 & in & 20\text{-D}, & N=15, & \text{mFE}=2.00\text{e7} \\ \\ \# & \text{ERT} & 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ 0 & 13e+1 & 10e+1 & 17e+1 & 1.0e7 \\ \\ \hline \\ & & & & & \\ \end{array} \\ \hline \\ f115 & in & 20\text{-D}, & N=15, & \text{mFE}=2.00\text{e7} \\ \\ \# & \text{ERT} & 10\% & 90\% & \text{RT}_{\text{succ}} \\ \hline \\ 1 & 2.9\text{e8} & 1.4\text{e8} & 3.e8 & 2.0\text{e7} \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ -3 \\ 1 \\ -5 \\ 1 \\ -8 \\ \Delta f \\ 1 \\ 1 \\ 1 \\ -5 \\ 1 \\ -8 \\ \Delta f \\ 10 \\ 1 \\ 1 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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$\begin{array}{c} \hline 10 \\ 1 \\ 1 \\ e^{-1} \\ 1e^{-3} \\ 1e^{-5} \\ 1e^{-8} \\ \hline 10 \\ 1 \\ 1e^{-1} \\ 1e^{-5} \\ 1e^{-8} \\ \hline 10 \\ 1 \\ 1e^{-3} \\ 1e^{-5} \\ 1e^{-8} \\ \hline \Delta f \\ 10 \\ 1 \\ 1 \\ \end{array}$	$\begin{array}{c} \textbf{j} & \textbf{i} & $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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$\begin{array}{c} \hline 10 \\ 1 \\ 1 \\ e^{-1} \\ 1e^{-3} \\ 1e^{-5} \\ e^{-8} \\ \hline \\ 10 \\ 1 \\ e^{-1} \\ 1e^{-3} \\ 1e^{-5} \\ 10 \\ 1 \\ e^{-1} \\ 1e^{-3} \\ 1e^{-5} \\ 10 \\ 1 \\ e^{-3} \\ 1e^{-1} \\ 1e^{-3} $	$\begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ 113 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RT_{succ} \\ 15 & 1.8e3 & 1.4e3 & 2.2e3 & 1.8e3 \\ 15 & 6.1e4 & 4.1e4 & 8.0e4 & 6.1e4 \\ 13 & 1.9e6 & 1.2e6 & 2.7e6 & 1.4e6 \\ 0 & 23e-3 & 96e-4 & 11e-2 & 2.2e6 \\ \vdots & \vdots & \vdots & \vdots \\ 115 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RT_{succ} \\ 15 & 1.1e2 & 7.8e1 & 1.4e2 & 1.1e2 \\ 15 & 5.0e3 & 3.7e3 & 7.6e3 & 5.6e3 \\ 15 & 1.2e5 & 7.5e4 & 1.6e5 & 1.2e5 \\ 2 & 3.6e7 & 1.9e7 & >7e7 & 5.0e6 \\ 2 & 3.6e7 & 1.9e7 & >7e7 & 5.0e6 \\ 2 & 3.6e7 & 1.9e7 & >7e7 & 5.0e6 \\ 15 & 6.1e4 & 406 & 3.0e6 \\ 117 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RT_{succ} \\ 12 & 3.5e6 & 2.7e6 & 4.4e6 & 3.0e6 \\ 1 & 7.1e7 & 3.3e7 & >7e7 & 5.0e6 \\ 0 & 67e-1 & 14e-1 & 12e+0 & 2.5e6 \\ 0 & & \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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$\begin{array}{c} \hline 1\\ \hline 1\\ 1\\ 1\\ e-1\\ 1\\ e-3\\ 1\\ e-5\\ 1\\ e-5\\ 1\\ e-5\\ 1\\ e-5\\ 1\\ e-5\\ 1\\ e-8\\ \hline 1\\ 1\\ e-3\\ 1\\ e-5\\ 1\\ e-8\\ \hline 1\\ e-8\\ \hline 1\\ e-8\\ \hline 1\\ e-8\\ 1\\ 1\\ e-8\\ 1\\ 1\\ e-8\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} \begin{array}{c} 10 & 15e+3 & 11e+3 & 20e+3 & 1.1e7 \\ \hline \\ 113 & 1n & 20-D, \ N=15, \ mFE=2.00e7 \\ \# \ ERT & 10\% & 90\% \ RT_{succ} \\ \hline 0 & 13e+1 & 10e+1 & 17e+1 & 1.0e7 \\ \hline \\ 120 & 13e+1 & 10e+1 & 17e+1 & 1.0e7 \\ \hline \\ 120 & 13e+1 & 10e+1 & 17e+1 & 1.0e7 \\ \hline \\ \# \ ERT & 10\% & 90\% \ RT_{succ} \\ \hline 1 & 2.9e8 & 1.4e8 & >3e8 & 2.0e7 \\ \hline \\ 0 & 14e+0 & 11e+0 & 17e+0 & 1.1e7 \\ \hline \\ \hline \\ 1117 & 120-D, \ N=15, \ mFE=2.00e7 \\ \hline \\ \# \ ERT & 10\% & 90\% \ RT_{succ} \\ \hline \\ 0 & 69e+2 & 53e+2 & 97e+2 & 1.3e7 \\ \hline \\ \hline \\ \hline \\ 1119 & 1n & 20-D, \ N=15, \ mFE=2.00e7 \\ \hline \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \hline 1\\ \hline 1\\ 1\\ 1\\ 1\\ e^{-1}\\ 1\\ e^{-3}\\ 1\\ e^{-5}\\ 1\\ 1\\ 1\\ e^{-5}\\ 1\\ 1\\ 1\\ e^{-5}\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\ 1\\$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} -\frac{1}{10} \\ 1 \\ 1e -1 \\ 1e -3 \\ 1e -5 \\ 1e -8 \\ 1e -5 \\ 1e -5 \\ 1e -8 \\ 1e -5 \\$	$\begin{array}{c} \textbf{15} 8.8e5 & \textbf{6.1e5} & \textbf{1.1e6} & \textbf{8.8e5} \\ \textbf{0} & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ \textbf{0} & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ \textbf{0} & \textbf{1} & \textbf{1} & \textbf{5-D}, \textbf{N=15}, \textbf{mFE=5}.00e6 \\ \# & \textbf{ERT} & 10\% & 90\% & \textbf{RTsucc} \\ \textbf{15} & \textbf{1.8e3} & \textbf{1.4e3} & 2.2e3 & \textbf{1.8e3} \\ \textbf{15} & \textbf{1.1e4} & \textbf{1.4e4} & \textbf{10e4} & \textbf{6.1e4} \\ \textbf{13} & \textbf{1.9e6} & \textbf{1.2e6} & 2.7e6 & \textbf{1.4e6} \\ \textbf{0} & 23e-3 & 96e-4 & 11e-2 & 2.2e6 \\ \textbf{0} & 23e-3 & 96e-4 & 11e-2 & 2.2e6 \\ \textbf{0} & \textbf{11} & \textbf{11} & \textbf{11e-2} & \textbf{2.2e6} \\ \textbf{115} & \textbf{1.5e3} & \textbf{1.4e2} & \textbf{11e-2} & \textbf{11e2} \\ \textbf{115} & \textbf{1.1e2} & 7.8e1 & \textbf{1.4e2} & \textbf{11e2} \\ \textbf{15} & \textbf{1.1e2} & 7.8e1 & \textbf{1.4e2} & \textbf{11e2} \\ \textbf{15} & \textbf{1.6e3} & \textbf{3.7e3} & 7.6e3 & 5.6e3 \\ \textbf{15} & \textbf{1.2e5} & 7.5e4 & \textbf{1.6e5} & \textbf{1.2e5} \\ \textbf{2} & \textbf{3.6e7} & \textbf{1.9e7} & \textbf{7e7} & 5.0e6 \\ \textbf{2} & \textbf{3.6e7} & \textbf{1.9e7} & \textbf{7e7} & 5.0e6 \\ \textbf{2} & \textbf{3.6e7} & \textbf{1.9e7} & \textbf{7e7} & 5.0e6 \\ \textbf{2} & \textbf{3.6e7} & \textbf{1.9e7} & \textbf{7e7} & 5.0e6 \\ \textbf{17} & \textbf{10} & \textbf{5-D}, \textbf{N=15}, \textbf{mFE=5.00e6} \\ \textbf{\# ERT} & 10\% & 90\% & \textbf{RTsucc} \\ \textbf{12} & \textbf{3.5e6} & \textbf{2.7e6} & 4.4e6 & \textbf{3.0e6} \\ \textbf{1} & \textbf{7.1e7} & \textbf{3.3e7} & \textbf{7e7} & 5.0e6 \\ \textbf{0} & 67e-1 & 14e-1 & 12e+0 & \textbf{2.5e6} \\ \textbf{0} & \textbf{0} & \textbf{0} & \textbf{1.6e} \\ \textbf{1} & \textbf{7.1e7} & \textbf{3.3e7} & \textbf{7e7} & \textbf{5.0e6} \\ \textbf{15} & \textbf{1.9e5} & \textbf{D, N=15}, \textbf{mFE=5.00e6} \\ \textbf{\# ERT} & 10\% & 90\% & \textbf{RTsucc} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.3e2} & \textbf{2.4e2} \\ \textbf{12} & \textbf{3.5e6} & \textbf{1.7e-1} & \textbf{2.7e6} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.3e2} & \textbf{2.4e2} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.3e2} & \textbf{2.4e2} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.3e2} & \textbf{2.4e2} \\ \textbf{15} & \textbf{1.8e2} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.3e2} & \textbf{2.4e2} \\ \textbf{15} & \textbf{1.8e2} \\ \textbf{15} & \textbf{1.8e2} & \textbf{1.8e2} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf{16} \\ \textbf{16} \\ \textbf{16} & \textbf{16} & \textbf{16} \\ \textbf{16} & \textbf$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} -\frac{1}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \\ \frac{\Delta f}{10} \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ \frac{\Delta f}{10} \\ \frac{\Delta f}{10$	$\begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e-1 & 22e-1 & 66e-1 & 2.8e6 \\ & & & & & & & & & & & & & & & & & & $	$\begin{array}{c} \textbf{f113 in 20-D, N=15, mFE=2.00e7} \\ \textbf{f113 in 20-D, N=15, mFE=2.00e7} \\ \textbf{\# ERT 10\% 90\% RT_{Succ}} \\ \textbf{0 } 13e+1 10e+1 17e+1 1.0e7} \\ \\ \\ \textbf{f115 in 20-D, N=15, mFE=2.00e7} \\ \textbf{\# ERT 10\% 90\% RT_{Succ}} \\ \textbf{1 } 2.9e8 1.4e8 > 3e8 2.0e7 \\ \textbf{0 } 14e+0 11e+0 17e+0 1.1e7 \\ \\ \\ \\ \\ \\ \textbf{f117 in 20-D, N=15, mFE=2.00e7} \\ \textbf{\# ERT 10\% 90\% RT_{Succ}} \\ \textbf{0 } 69e+2 53e+2 97e+2 1.3e7 \\ $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} -\frac{1}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \\ \frac{\Delta f}{10} \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ 1 \\ le-1 \\ le-3 \\ le-5 \\ le-8 \\ \frac{\Delta f}{10} \\ \Delta f$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} \textbf{f113 in 20-D, N=15, mFE=2.00e7} \\ \textbf{f113 in 20-D, N=15, mFE=2.00e7} \\ \textbf{\# ERT 10\% 90\% RT_{succ}} \\ \textbf{0 } 13e+1 10e+1 17e+1 1.0e7} \\ \textbf{0 } 13e+1 10e+1 17e+1 1.0e7} \\ \textbf{0 } 13e+1 10e+1 17e+1 1.0e7} \\ \textbf{0 } 12e+1 10e+1 11e+1 1.0e7} \\ \textbf{0 } 12e+1 10e+1 11e+1 1.0e7} \\ \textbf{0 } 12e+1 11e+1 1.0e7 \\ \textbf{0 } 12e+1 11e+1 11e+1 11e+1 1.0e7 \\ \textbf{0 } 12e+1 11e+1 11e+1 11e+1 1.0e7 \\ \textbf{0 } 12e+1 11e+1 11e+$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} -\frac{1}{10} \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ -3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ $	$\begin{array}{c} 15 & 8.8e5 & 6.1e5 & 1.1e6 & 8.8e5 \\ 0 & 45e^{-1} & 22e^{-1} & 66e^{-1} & 2.8e6 \\ 0 & 45e^{-1} & 22e^{-1} & 66e^{-1} & 2.8e6 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 113 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RTsucc \\ 15 & 1.8e3 & 1.4e3 & 2.2e3 & 1.8e3 \\ 15 & 6.1e4 & 4.1e4 & 8.0e4 & 6.1e4 \\ 13 & 1.9e6 & 1.2e6 & 2.7e6 & 1.4e6 \\ 0 & 23e^{-3} & 96e^{-4} & 11e^{-2} & 2.2e6 \\ \vdots & \vdots & \vdots & \vdots \\ 115 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RTsucc \\ 15 & 1.1e2 & 7.8e1 & 1.4e2 & 1.1e2 \\ 15 & 5.6e3 & 3.7e3 & 7.6e3 & 5.6e3 \\ 15 & 1.1e2 & 7.8e1 & 1.4e2 & 1.1e2 \\ 15 & 5.6e3 & 3.7e3 & 7.6e3 & 5.6e3 \\ 15 & 1.1e2 & 7.8e1 & 1.4e^{-3} & 1.2e5 \\ 2 & 3.6e7 & 1.9e7 & >7e7 & 5.0e6 \\ 2 & 3.6e7 & 1.9e7 & >7e7 & 5.0e6 \\ 0 & 96e^{-4} & 40e^{-3} & 1.2e6 \\ 117 & in & 5-D, N=15, mFE=5.00e6 \\ \# & ERT & 10\% & 90\% & RTsucc \\ 15 & 1.8e2 & 1.3e2 & 2.4e2 & 1.8e2 \\ 15 & 7.7e3 & 5.6e3 & 1.0e4 & 7.7e3 \\ 15 & 2.9e5 & 2.2e5 & 3.7e5 & 2.9e5 \\ 0 & 13e^{-3} & 53e^{-3} & 1.0e4 & 7.7e3 \\ 15 & 2.9e5 & 2.2e5 & 3.7e5 & 2.9e5 \\ 0 & 13e^{-3} & 53e^{-3} & 1.0e4 & 7.7e3 \\ 15 & 2.9e5 & 2.2e5 & 3.7e5 & 2.9e5 \\ 0 & 13e^{-3} & 53e^{-3} & 2.0e6 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Table 1: Shown are, for functions $f_{101}-f_{120}$ and for a given target difference to the optimal function value Δf : the number of successful trials (#); the expected running time to surpass $f_{opt} + \Delta f$ (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (\mathbf{RT}_{succ}). If $f_{opt} + \Delta f$ was never reached, figures in *italics* denote the best achieved Δf -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.



Figure 2: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left subplots) or versus Δf (right subplots). The thick red line represents the best achieved results. Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension D, to fall below $f_{opt} + \Delta f$ with $\Delta f = 10^k$, where k is the first value in the legend. Right subplots: ECDF of the best achieved Δf divided by 10^k (upper left lines in continuation of the left subplot), and best achieved Δf divided by 10^{-8} for running times of D, 10D, 100D... function evaluations (from right to left cycling blackcyan-magenta). Top row: all results from all functions; second row: moderate noise functions; third row: severe noise functions; fourth row: severe noise and highly-multimodal functions. The legends indicate the number of functions that were solved in at least one trial. FEvals denotes number of function evaluations, Dand DIM denote search space dimension, and Δf and Df denote the difference to the optimal function value.

Δf	<i>f</i> 121 in 5-D , N=15, mFE=5.00 e6 # ERT 10% 90% RT _{succ}	f_{121} in 20-D, N=15, mFE=2.00 e7 # ERT 10% 90% RT _{succ}	$\Delta f = \frac{f_{122} \text{ in } 5\text{-D}, \text{ N}=15, \text{ mFE}=5.00 \text{ e6}}{\# \text{ ERT } 10\% 90\% \text{ RT}_{\text{succ}}}$	f_{122} in 20-D, N=15, mFE=2.00 e7 # ERT 10% 90% RT _{succ}
10	15 2.6e1 2.1e1 3.2e1 2.6e1	15 4.1e3 3.0e3 5.3e3 4.1e3	10 15 1.8e2 1.3e2 2.2e2 1.8e2	15 1.4e5 6.1e4 2.2e5 1.4e5
1	15 5.0e2 3.6e2 6.5e2 5.0e2	0 16e-1 12e-1 21e-1 7.9e6	1 15 1.2e5 9.2e4 1.6e5 1.2e5	0 57e-1 39e-1 62e-1 7.9e6
$1\mathrm{e}-1$	15 1.3e4 1.0e4 1.7e4 1.3e4		1e-1 0 $24e-2$ $17e-2$ $40e-2$ $1.6e6$	
$1\mathrm{e}-3$	0 51e-4 28e-4 80e-4 2.5e6		1e-3	
$1\mathrm{e}-5$			1e-5	
$1\mathrm{e}-8$			1e-8	
	f123 in 5-D, N=15, mFE=5.00e6	f123 in 20-D, N=15, mFE=2.00e7	f124 in 5-D, N=15, mFE=5.00e6	f124 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	Δf # ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}
10	15 2.5e2 1.6e2 3.4e2 2.5e2	15 2.1e5 1.4e5 2.9e5 2.1e5	10 15 4.6e1 1.8e1 7.5e1 4.6e1	15 1.3e4 8.4e3 1.7e4 1.3e4
1	15 3.7e5 2.6e5 4.9e5 3.7e5	0 64e-1 59e-1 68e-1 7.9e6	1 15 7.0e3 4.5e3 9.8e3 7.0e3	0 36e-1 32e-1 43e-1 7.1e6
$1\mathrm{e}-1$	0 59e-2 45e-2 63e-2 2.2e6		1e-1 2 3.6e7 1.9e7 >7e7 5.0e6	
1e - 3			1e-3 0 $12e-2$ $92e-3$ $15e-2$ $2.0e6$	
$1\mathrm{e}-5$			1e-5	
$1\mathrm{e}-8$			1e-8	
	f125 in 5-D, N=15, mFE=5.00e6	f125 in 20-D, N=15, mFE=2.00e7	f126 in 5-D, N=15, mFE=5.00e6	f126 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT } 10\% 90\% \text{ RT}_{succ}$	# ERT 10% 90% RT _{succ}
10	15 2.5e0 1.1e0 4.0e0 2.5e0	15 1.0e0 1.0e0 1.0e0 1.0e0	10 15 1.8e1 2.9e0 3.4e1 1.8e1	15 1.0e0 1.0e0 1.0e0 1.0e0
1	15 2.1e2 1.3e2 3.0e2 2.1e2	15 6.5e5 5.0e5 8.2e5 6.5e5	1 15 4.3e2 2.7e2 6.1e2 4.3e2	15 3.1e6 2.1e6 4.1e6 3.1e6
$1\mathrm{e}-1$	15 3.3e4 2.3e4 4.3e4 3.3e4	0 75e-2 66e-2 77e-2 1.3e7	1e-1 15 2.4e5 1.7e5 3.0e5 2.4e5	0 85e-2 77e-2 90e-2 8.9e6
$1\mathrm{e}-3$	0 13e-3 71e-4 23e-3 2.0e6		1e-3 0 27e-3 15e-3 41e-3 2.0e6	
$1\mathrm{e}-5$			1e-5	
$1\mathrm{e}-8$			1e-8	
	f127 in 5-D, N=15, mFE=5.00e6	f127 in 20-D, N=15, mFE=2.00e7	f128 in 5-D, N=15, mFE=5.00e6	f128 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{succ}$	# ERT 10% 90% RT _{succ}
10	15 1.1e0 1.0e0 1.3e0 1.1e0	15 1.3e0 1.0e0 1.5e0 1.3e0	10 15 8.4e2 6.4e2 1.0e3 8.4e2	0 34e+0 24e+0 48e+0 7.1e6
1	15 6.5e1 3.1e1 1.0e2 6.5e1	15 2.8e4 1.8e4 3.8e4 2.8e4	1 15 2.5e4 1.9e4 3.0e4 2.5e4	
$1\mathrm{e}-1$	15 3.6e4 2.5e4 4.9e4 3.6e4	0 62e-2 50e-2 66e-2 1.1e7	1e-1 15 6.5e4 4.9e4 8.3e4 6.5e4	
1e-3	0 24e-3 15e-3 30e-3 2.5e6		1e-3 15 3.2e5 2.2e5 4.3e5 3.2e5	
$1\mathrm{e}-5$			1e-5 14 2.3e6 1.7e6 3.0e6 2.1e6	
$1\mathrm{e}-8$			1e-8 0 $17e-7$ $46e-9$ $68e-7$ $2.5e6$	
	f129 in 5-D, N=15, mFE=5.00e6	f129 in 20-D, N=15, mFE=2.00e7	f130 in 5-D, N=15, mFE=5.00e6	f130 in 20-D, N=15, mFE=2.00e7
Δf	# ERT 10% 90% RT _{SUCC}	# ERT 10% 90% RT _{SUCC}	$\Delta f \# \text{ ERT} 10\% 90\% \text{ RT}_{SUCC}$	# ERT 10% 90% RT _{SUCC}
10	15 1.9e3 1.5e3 2.3e3 1.9e3	0 48e+0 34e+0 56e+0 1.0e7	10 15 1.8e2 1.1e2 2.5e2 1.8e2	15 2.1e4 1.4e4 2.7e4 2.1e4
1	15 7.3e4 5.2e4 9.2e4 7.3e4		1 15 4.7e3 3.4e3 6.0e3 4.7e3	10 1.8e7 1.2e7 2.8e7 9.2e6
$1\mathrm{e}-1$	15 5.3e5 4.3e5 6.4e5 5.3e5		1e-1 15 9.3e3 7.3e3 1.1e4 9.3e3	0 74e-2 46e-2 16e-1 7.1e6
$1\mathrm{e}-3$	0 60e-4 24e-4 18e-3 2.2e6		1e-3 15 2.3e5 1.4e5 3.3e5 2.3e5	
$1\mathrm{e}-5$			1e-5 5 1.3e7 8.6e6 2.3e7 4.3e6	
$1\mathrm{e}-8$			1e-8 0 57e-6 31e-7 13e-5 2.5e6	

Table 2: Shown are, for functions f_{121} - f_{130} and for a given target difference to the optimal function value Δf : the number of successful trials (#); the expected running time to surpass $f_{opt} + \Delta f$ (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (\mathbf{RT}_{succ}). If $f_{opt} + \Delta f$ was never reached, figures in *italics* denote the best achieved Δf -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.