

# AMaLGaM IDEAs in Noisy Black-Box Optimization Benchmarking

Peter A.N. Bosman  
Centre for Mathematics and  
Computer Science  
P.O. Box 94079  
1090 GB Amsterdam  
The Netherlands  
Peter.Bosman@cwi.nl

Jörn Grahl  
Johannes Gutenberg  
University Mainz  
Dept. of Information Systems  
& Business Administration  
Jakob Welder-Weg 9  
D-55128 Mainz, Germany  
grahl@uni-mainz.de

Dirk Thierens  
Utrecht University  
Dept. of Information and  
Computing Sciences  
P.O. Box 80089  
3508 TB Utrecht  
The Netherlands  
Dirk.Thierens@cs.uu.nl

## ABSTRACT

This paper describes the application of a Gaussian Estimation-of-Distribution (EDA) for real-valued optimization to the noisy part of a benchmark introduced in 2009 called BBOB (Black-Box Optimization Benchmarking). Specifically, the EDA considered here is the recently introduced parameter-free version of the Adapted Maximum-Likelihood Gaussian Model Iterated Density-Estimation Evolutionary Algorithm (AMaLGaM-IDEA). Also the version with incremental model building (iAMaLGaM-IDEA) is considered.

## Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization Global Optimization, Unconstrained Optimization; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

## General Terms

Algorithms

## Keywords

Benchmarking, Black-box optimization, Evolutionary computation

## 1. METHOD

Estimation-of-distribution algorithms attempt to automatically exploit features of a problem's structure by probabilistically modeling the search space based on previously evaluated solutions and generating new solutions by sampling the probabilistic model.

The EDA considered here is the Adapted Maximum-Likelihood Gaussian Model Iterated Density-Estimation Evolutionary Algorithm (AMaLGaM-IDEA, or AMaLGaM for short). In AMaLGaM, the probability distribution used is the normal, also known as the Gaussian, distribution. This

Permission to make digital or hard copies of all or part of this work for personal or classroom use is granted without fee provided that copies are not made or distributed for profit or commercial advantage and that copies bear this notice and the full citation on the first page. To copy otherwise, to republish, to post on servers or to redistribute to lists, requires prior specific permission and/or a fee.

GECCO'09, July 8–12, 2009, Montréal Québec, Canada.  
Copyright 2009 ACM 978-1-60558-505-5/09/07 ...\$5.00.

EDA uses maximum-likelihood estimates for the mean and the covariance matrix, estimated from the selected solutions. It has a mechanism that scales up the covariance matrix when required to prevent premature convergence on slopes. It furthermore has a mechanism that anticipates the mean shift in the next generation to speed up descent (in case of minimization) along slopes. In another paper [1], AMaLGaM, and its incremental-learning variant iAMaLGaM, were tested on the noiseless variant of the BBOB benchmark. Due to space restrictions, we refer the interested reader for more details on AMaLGaM such as the parameters and other settings as well as the CPU timing experiment to the other workshop paper.

## 2. RESULTS AND CONCLUSION

Results from experiments according to [3] on the benchmark functions given in [2, 4] are presented in Figures 1 and 2 and in Tables 1 and 3 for AMaLGaM and in Figures 3 and 4 and in Tables 2 and 4 for iAMaLGaM.

Problems with severe noise and multimodality appear to be the hardest for (i)AMaLGaM. Even within  $10^6 D$  evaluations the optimum cannot be found within a desirable precision for larger  $D$ . The difference between AMaLGaM and iAMaLGaM is not large. Most likely due to the larger base population-size, AMaLGaM performs slightly better. The difference is larger for the multi-modal problems, which is consistent with earlier findings.

## 3. REFERENCES

- [1] P. A. N. Bosman, J. Grahl, and D. Thierens. AMaLGaM IDEAs in noiseless black-box optimization benchmarking. In A. Auger et al., editors, *Proceedings of the Black Box Optimization Benchmarking BBOB Workshop at the Genetic and Evolutionary Computation Conference — GECCO-2009*, New York, New York, 2009. ACM Press. (*To Appear*).
- [2] S. Finck, N. Hansen, R. Ros, and A. Auger. Real-parameter black-box optimization benchmarking 2009: Presentation of the noisy functions. Technical Report 2009/20, Research Center PPE, 2009.
- [3] N. Hansen, A. Auger, S. Finck, and R. Ros. Real-parameter black-box optimization benchmarking 2009: Experimental setup. Technical Report RR-6828, INRIA, 2009.
- [4] N. Hansen, S. Finck, R. Ros, and A. Auger. Real-parameter black-box optimization benchmarking 2009: Noisy functions definitions. Technical Report RR-6829, INRIA, 2009.

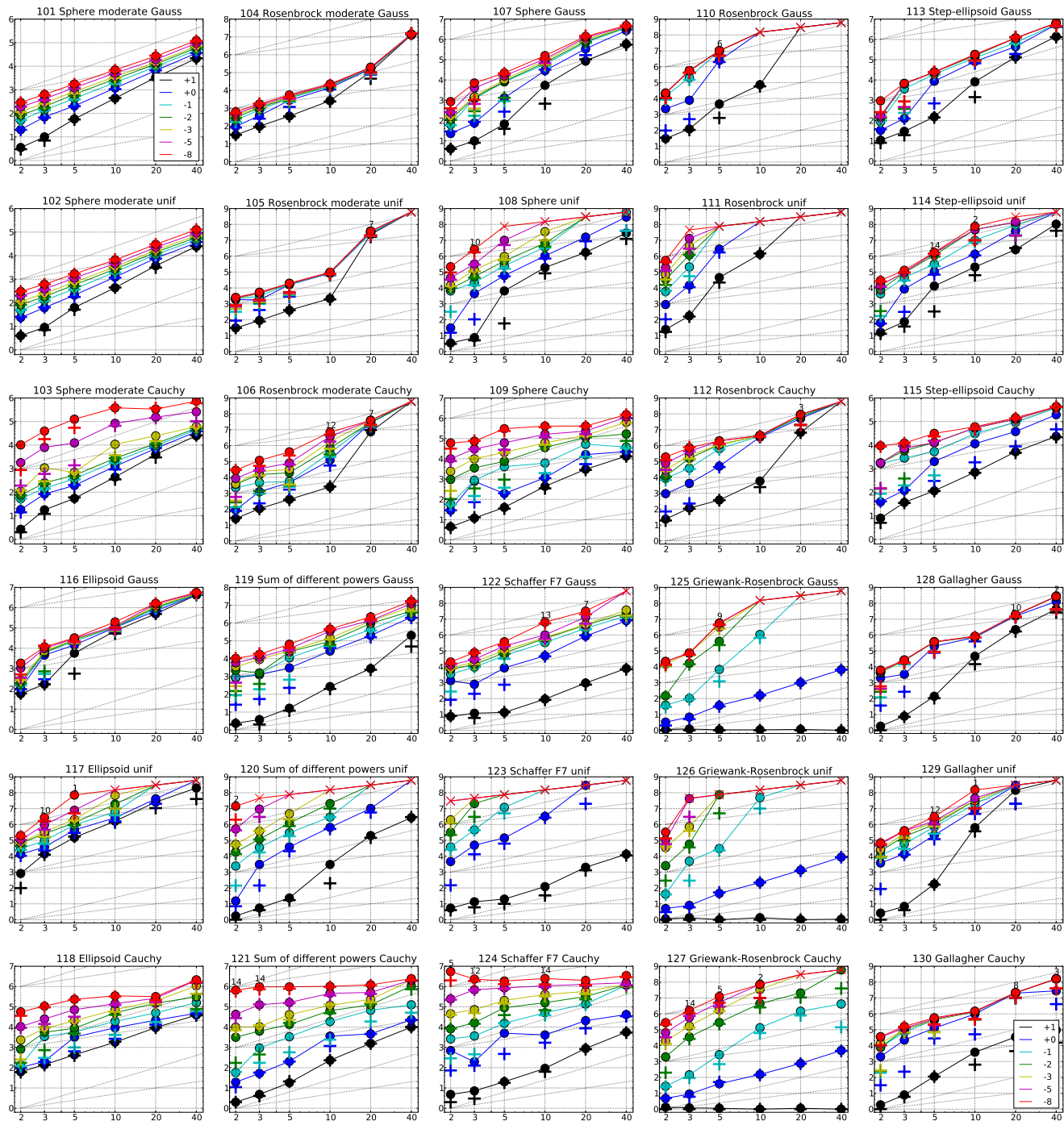


Figure 1: AMaLGaM: Expected Running Time (ERT, ●) to reach  $f_{\text{opt}} + \Delta f$  and median number of function evaluations of successful trials (+), shown for  $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$  (the exponent is given in the legend of  $f_{101}$  and  $f_{130}$ ) versus dimension in log-log presentation. The  $\text{ERT}(\Delta f)$  equals to  $\#FEs(\Delta f)$  divided by the number of successful trials, where a trial is successful if  $f_{\text{opt}} + \Delta f$  was surpassed during the trial. The  $\#FEs(\Delta f)$  are the total number of function evaluations while  $f_{\text{opt}} + \Delta f$  was not surpassed during the trial from all respective trials (successful and unsuccessful), and  $f_{\text{opt}}$  denotes the optimal function value. Crosses (×) indicate the total number of function evaluations  $\#FEs(-\infty)$ . Numbers above ERT-symbols indicate the number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

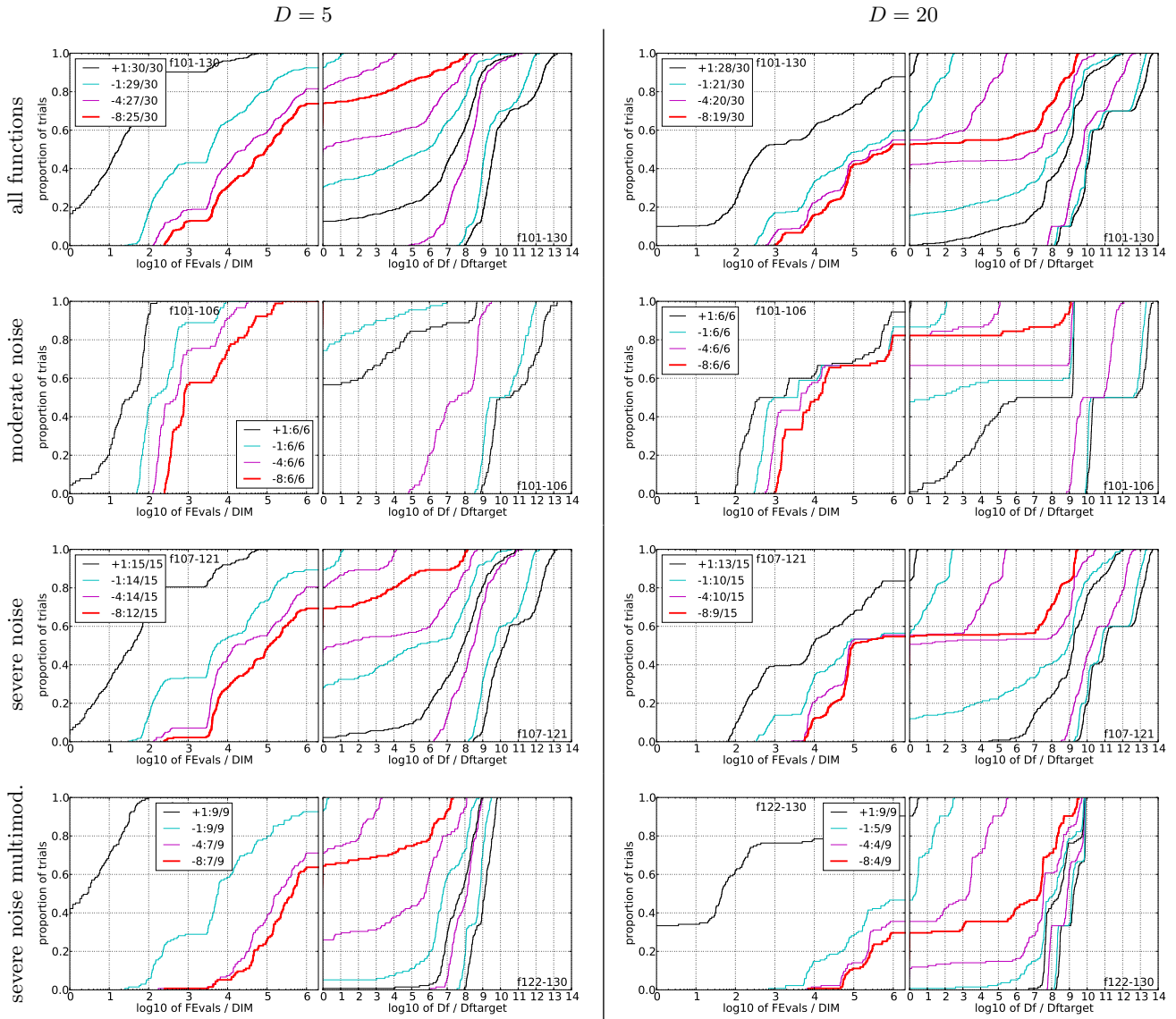


Figure 2: AMaLGaM: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left) or  $\Delta f$ . Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension  $D$ , to fall below  $f_{\text{opt}} + \Delta f$  with  $\Delta f = 10^k$ , where  $k$  is the first value in the legend. Right subplots: ECDF of the best achieved  $\Delta f$  divided by  $10^k$  (upper left lines in continuation of the left subplot), and best achieved  $\Delta f$  divided by  $10^{-8}$  (from right to left cycling black-cyan-magenta). Top row: all results from all functions; second row: moderate noise functions; third row: severe noise functions; fourth row: severe noise and highly-multimodal functions. The legends indicate the number of functions that were solved in at least one trial. FEvals denotes number of function evaluations,  $D$  and DIM denote search space dimension, and  $\Delta f$  and Df denote the difference to the optimal function value.

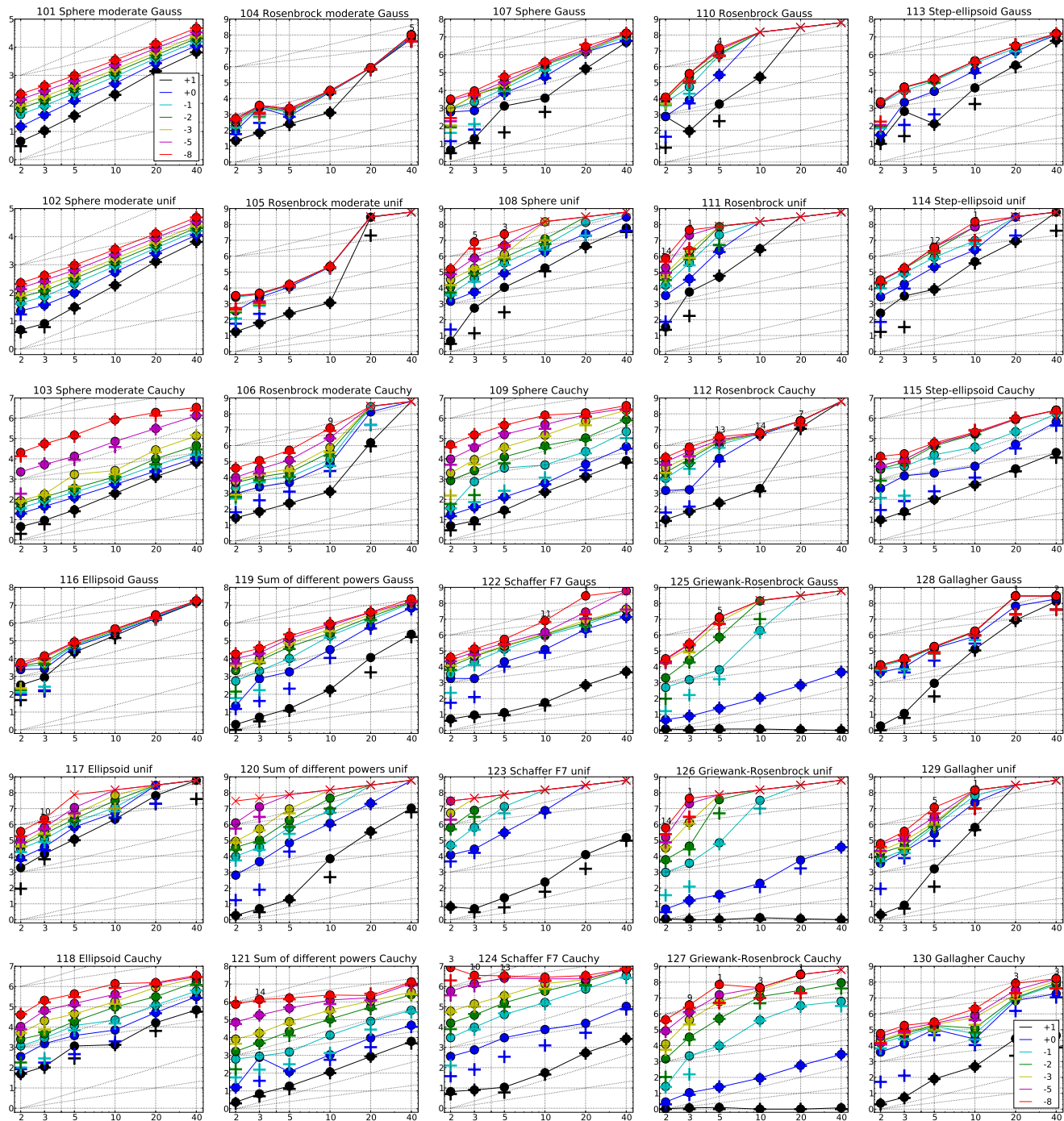


Figure 3: iAMaLGaM: Expected Running Time (ERT, ●) to reach  $f_{\text{opt}} + \Delta f$  and median number of function evaluations of successful trials (+), shown for  $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$  (the exponent is given in the legend of  $f_{101}$  and  $f_{130}$ ) versus dimension in log-log presentation. The  $\text{ERT}(\Delta f)$  equals to  $\#FEs(\Delta f)$  divided by the number of successful trials, where a trial is successful if  $f_{\text{opt}} + \Delta f$  was surpassed during the trial. The  $\#FEs(\Delta f)$  are the total number of function evaluations while  $f_{\text{opt}} + \Delta f$  was not surpassed during the trial from all respective trials (successful and unsuccessful), and  $f_{\text{opt}}$  denotes the optimal function value. Crosses (×) indicate the total number of function evaluations  $\#FEs(-\infty)$ . Numbers above ERT-symbols indicate the number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

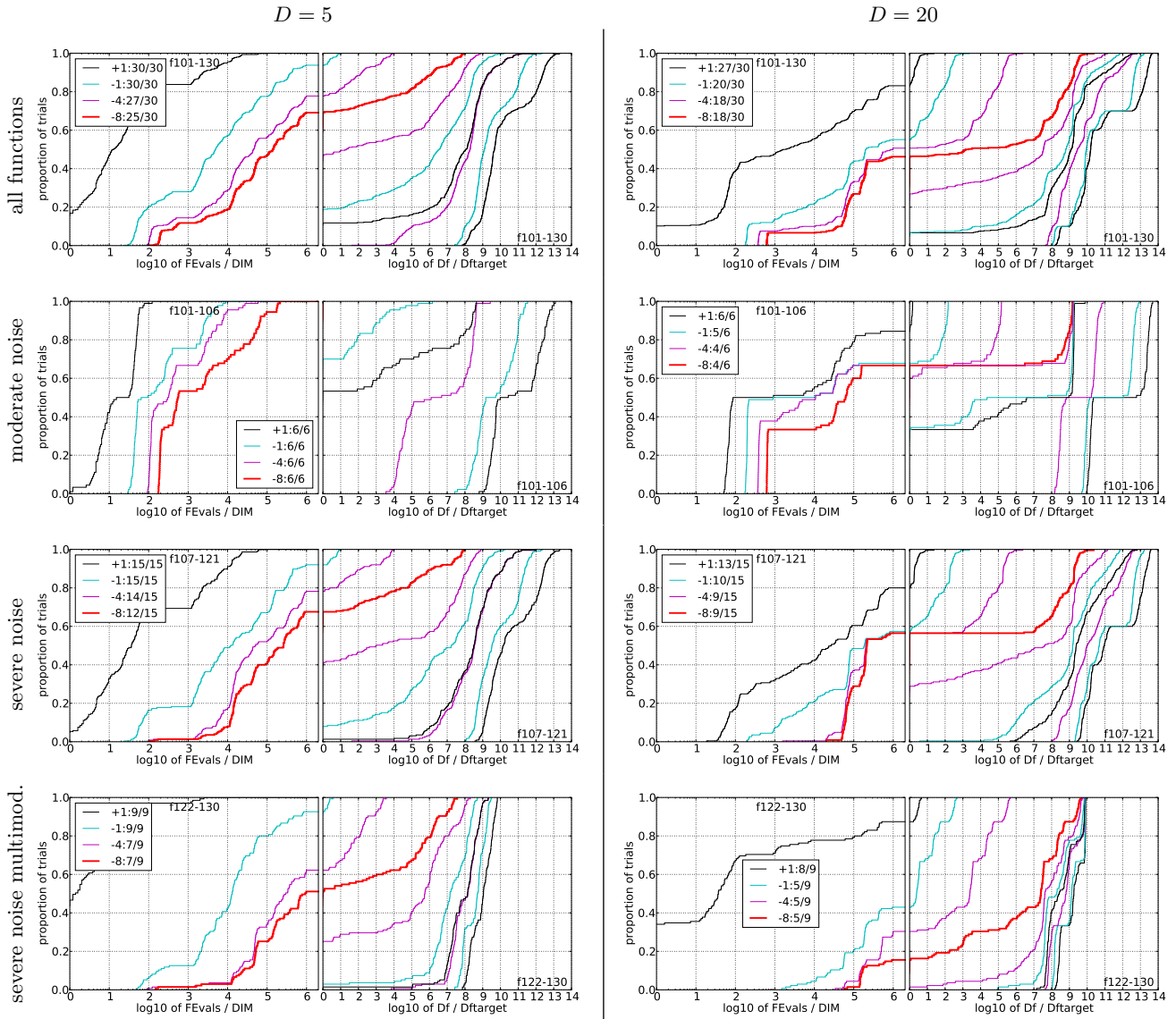


Figure 4: iAMaLGaM: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left) or  $\Delta f$ . Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension  $D$ , to fall below  $f_{\text{opt}} + \Delta f$  with  $\Delta f = 10^k$ , where  $k$  is the first value in the legend. Right subplots: ECDF of the best achieved  $\Delta f$  divided by  $10^k$  (upper left lines in continuation of the left subplot), and best achieved  $\Delta f$  divided by  $10^{-8}$  (from right to left cycling black-cyan-magenta). Top row: all results from all functions; second row: moderate noise functions; third row: severe noise functions; fourth row: severe noise and highly-multimodal functions. The legends indicate the number of functions that were solved in at least one trial. FEvals denotes number of function evaluations,  $D$  and DIM denote search space dimension, and  $\Delta f$  and Df denote the difference to the optimal function value.

$f_{101}$ in 5-D, N=15, mFE=2892					$f_{101}$ in 20-D, N=15, mFE=31809					$f_{102}$ in 5-D, N=15, mFE=2206					$f_{102}$ in 20-D, N=15, mFE=36921						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	5.8e1	4.5e1	7.1e1	5.8e1	15	3.4e3	2.9e3	3.8e3	3.4e3	15	6.3e1	4.6e1	8.0e1	6.3e1	15	3.7e3	3.2e3	4.2e3	3.7e3	
1	15	2.1e2	1.8e2	2.2e2	2.1e2	15	6.5e3	6.0e3	7.0e3	6.5e3	1	15	2.1e2	1.8e2	2.4e2	2.1e2	15	7.8e3	7.1e3	8.4e3	7.8e3
1e-1	15	4.3e2	3.7e2	4.9e2	4.3e2	15	9.6e3	8.7e3	1.0e4	9.6e3	1e-1	15	3.8e2	3.4e2	4.2e2	3.8e2	15	1.1e4	1.0e4	1.2e4	1.1e4
1e-3	15	8.4e2	7.5e2	9.3e2	8.4e2	15	1.5e4	1.4e4	1.6e4	1.5e4	1e-3	15	7.5e2	7.0e2	8.1e2	7.5e2	15	1.7e4	1.6e4	1.8e4	1.7e4
1e-5	15	1.2e3	1.1e3	1.4e3	1.2e3	15	1.9e4	1.8e4	2.1e4	1.9e4	1e-5	15	1.1e3	1.0e3	1.2e3	1.1e3	15	2.2e4	2.1e4	2.4e4	2.2e4
1e-8	15	1.8e3	1.6e3	1.9e3	1.8e3	15	2.7e4	2.6e4	2.8e4	2.7e4	1e-8	15	1.7e3	1.6e3	1.8e3	1.7e3	15	3.0e4	2.9e4	3.2e4	3.0e4
$f_{103}$ in 5-D, N=15, mFE=651264					$f_{103}$ in 20-D, N=15, mFE=923247					$f_{104}$ in 5-D, N=15, mFE=31356					$f_{104}$ in 20-D, N=15, mFE=334844						
10	15	5.4e1	4.5e1	6.4e1	5.4e1	15	4.0e3	3.4e3	4.6e3	4.0e3	10	15	3.6e2	3.3e2	3.9e2	3.6e2	15	1.1e5	8.3e4	1.4e5	1.1e5
1	15	1.9e2	1.8e2	2.1e2	1.9e2	15	7.2e3	6.5e3	7.8e3	7.2e3	1	15	2.8e3	1.0e3	4.5e3	2.8e3	15	1.6e5	1.3e5	1.9e5	1.6e5
1e-1	15	3.7e2	3.5e2	4.0e2	3.7e2	15	9.5e3	8.7e3	1.0e4	9.5e3	1e-1	15	3.6e3	1.8e3	5.5e3	3.6e3	15	1.7e5	1.4e5	2.0e5	1.7e5
1e-3	15	6.9e2	6.5e2	7.4e2	6.9e2	15	2.5e4	1.4e4	3.5e4	2.5e4	1e-3	15	4.5e3	2.5e3	6.4e3	4.5e3	15	1.8e5	1.5e5	2.2e5	1.8e5
1e-5	15	1.2e4	8.2e3	1.7e4	1.2e4	15	1.5e5	1.2e5	1.9e5	1.5e5	1e-5	15	1.9e3	3.0e3	7.0e3	4.9e3	15	1.9e5	1.5e5	2.2e5	1.9e5
1e-8	15	1.3e5	7.6e4	1.8e5	1.3e5	15	3.4e5	2.7e5	4.0e5	3.4e5	1e-8	15	5.5e3	3.6e3	7.6e3	5.5e3	15	2.0e5	1.6e5	2.3e5	2.0e5
$f_{105}$ in 5-D, N=15, mFE=48000					$f_{105}$ in 20-D, N=15, mFE=2.00e7					$f_{106}$ in 5-D, N=15, mFE=1.24e6					$f_{106}$ in 20-D, N=15, mFE=2.00e7						
10	15	3.9e2	3.6e2	4.3e2	3.9e2	10	2.3e7	1.9e7	3.0e7	1.6e7	10	15	4.1e2	3.7e2	4.5e2	4.1e2	15	7.4e6	6.1e6	8.6e6	7.4e6
1	15	1.6e4	1.0e4	2.2e4	1.6e4	9	2.8e7	2.2e7	3.8e7	1.8e7	1	15	4.7e3	1.5e3	7.8e3	4.7e3	9	2.7e7	2.1e7	3.8e7	1.6e7
1e-1	15	1.7e4	1.2e4	2.3e4	1.7e4	9	2.8e7	2.3e7	3.8e7	1.8e7	1e-1	15	5.6e3	2.4e3	8.9e3	5.6e3	9	2.9e7	2.2e7	3.9e7	1.7e7
1e-3	15	1.8e4	1.3e4	2.4e4	1.8e4	7	3.7e7	2.7e7	5.6e7	1.8e7	1e-3	15	3.1e4	1.7e4	4.7e4	3.1e4	7	3.9e7	2.8e7	5.8e7	1.8e7
1e-5	15	1.9e4	1.3e4	2.5e4	1.9e4	7	3.7e7	2.8e7	5.7e7	1.8e7	1e-5	15	8.0e4	6.4e4	9.6e4	8.0e4	7	3.9e7	2.8e7	5.8e7	1.8e7
1e-8	15	2.0e4	1.4e4	2.5e4	2.0e4	7	3.7e7	2.8e7	5.9e7	1.9e7	1e-8	15	4.0e5	2.8e5	5.1e5	4.0e5	7	3.9e7	2.9e7	5.7e7	1.8e7
$f_{107}$ in 5-D, N=15, mFE=33716					$f_{107}$ in 20-D, N=15, mFE=1.93e6					$f_{108}$ in 5-D, N=15, mFE=5.01e6					$f_{108}$ in 20-D, N=15, mFE=2.00e7						
10	15	6.7e1	3.8e1	9.9e1	6.7e1	15	8.5e4	6.2e4	1.1e5	8.5e4	10	15	6.5e3	3.0e3	1.0e4	6.5e3	15	1.7e6	1.3e6	2.1e6	1.7e6
1	15	1.3e3	3.0e2	2.3e3	1.3e3	15	3.4e5	2.1e5	4.9e5	3.4e5	1	15	6.0e4	4.2e4	7.7e4	6.0e4	10	1.6e7	1.1e7	2.3e7	1.0e7
1e-1	15	8.1e3	5.5e3	1.1e4	8.1e3	15	7.0e5	5.3e5	8.6e5	7.0e5	1e-1	15	2.5e5	1.9e5	3.0e5	2.5e5	0	<i>48e-2</i>	<i>18e-2</i>	<i>19e-1</i>	7.9e6
1e-3	15	1.0e4	7.4e3	1.3e4	1.0e4	15	9.9e5	8.3e5	1.2e6	9.9e5	1e-3	15	9.6e5	6.5e5	1.3e6	9.6e5					
1e-5	15	1.6e4	1.3e4	1.9e4	1.6e4	15	1.2e6	1.1e6	1.4e6	1.2e6	1e-5	6	9.9e6	6.5e6	1.7e7	3.4e6					
1e-8	15	2.2e4	2.0e4	2.4e4	2.2e4	15	1.4e6	1.3e6	1.5e6	1.4e6	1e-8	0	<i>20e-6</i>	<i>57e-9</i>	<i>16e-5</i>	2.2e6					
$f_{109}$ in 5-D, N=15, mFE=714314					$f_{109}$ in 20-D, N=15, mFE=1.12e6					$f_{110}$ in 5-D, N=15, mFE=5.01e6					$f_{110}$ in 20-D, N=15, mFE=2.00e7						
10	15	4.0e1	3.1e1	5.0e1	4.0e1	15	3.0e3	2.8e3	3.3e3	3.0e3	10	15	4.5e3	1.8e3	7.4e3	4.5e3	15	<i>18e+0</i>	<i>17e+0</i>	<i>18e+0</i>	1.6e7
1	15	1.9e2	1.8e2	2.1e2	1.9e2	15	1.6e4	6.5e3	2.7e4	1.6e4	1	13	2.5e6	1.7e6	3.4e6	1.9e6					
1e-1	15	4.1e3	3.7e2	7.3e3	4.1e3	15	5.2e4	3.5e4	7.0e4	5.2e4	1e-1	6	1.0e7	7.0e6	1.7e7	4.2e6					
1e-3	15	2.1e4	1.8e4	2.4e4	2.1e4	15	1.4e5	1.2e5	1.6e5	1.4e5	1e-3	6	1.0e7	7.1e6	1.7e7	4.3e6					
1e-5	15	6.2e4	4.3e4	8.0e4	6.2e4	15	2.3e5	1.9e5	2.8e5	2.3e5	1e-5	6	1.0e7	7.1e6	1.7e7	4.3e6					
1e-8	15	3.0e5	2.3e5	3.8e5	3.0e5	15	4.1e5	3.3e5	5.0e5	4.1e5	1e-8	6	1.0e7	7.1e6	1.6e7	4.3e6					
$f_{111}$ in 5-D, N=15, mFE=5.01e6					$f_{111}$ in 20-D, N=15, mFE=2.00e7					$f_{112}$ in 5-D, N=15, mFE=3.58e6					$f_{112}$ in 20-D, N=15, mFE=2.00e7						
10	15	4.5e4	2.8e4	6.4e4	4.5e4	0	<i>23e+0</i>	<i>20e+0</i>	<i>24e+0</i>	1.0e7	10	15	3.7e2	3.4e2	4.0e2	3.7e2	15	6.7e6	6.3e6	7.2e6	6.7e6
1	12	2.8e6	1.9e6	3.8e6	2.2e6						1	15	5.0e4	3.4e4	6.6e4	5.0e4	5	5.0e7	3.4e7	8.9e7	1.8e7
1e-1	0	<i>53e-2</i>	<i>17e-2</i>	<i>10e-1</i>	2.0e6						1e-1	15	6.3e5	4.7e5	8.0e5	6.3e5	4	6.4e7	4.1e7	1.3e8	1.7e7
1e-3											1e-3	15	1.2e6	8.9e5	1.5e6	1.2e6	3	9.0e7	5.1e7	2.7e8	1.7e7
1e-5											1e-5	15	2.0e6	1.6e6	2.3e6	2.0e6	3	9.0e7	5.2e7	2.8e8	1.7e7
1e-8											1e-8	15	2.0e6	1.7e6	2.3e6	2.0e6	3	9.0e7	5.3e7	2.7e8	1.7e7
$f_{113}$ in 5-D, N=15, mFE=66491					$f_{113}$ in 20-D, N=15, mFE=6.64e6					$f_{114}$ in 5-D, N=15, mFE=5.00e6					$f_{114}$ in 20-D, N=15, mFE=2.00e7						
10	15	1.5e2	1.3e2	1.8e2	1.5e2	15	1.4e5	1.0e5	1.7e5	1.4e5	10	15	1.3e4	6.2e3	2.0e4	1.3e4	15	2.6e6	2.2e6	2.9e6	2.6e6
1	15	8.7e3	4.4e3	1.3e4	8.7e3	15	4.4e5	3.2e5	5.7e5	4.4e5	1	15	1.0e5	7.2e4	1.4e5	1.0e5	6	3.8e7	2.5e7	6.5e7	1.3e7
1e-1	15	1.9e4	1.4e4	2.5e4	1.9e4	15	7.0e5	5.2e5	8.6e5	7.0e5	1e-1	15	3.2e5	2.5e5	4.0e5	3.2e5	3	9.0e7	5.2e7	2.8e8	1.7e7
1e-3	15	2.4e4	1.9e4	3.0e4	2.4e4	15	1.2e6	1.0e6	1.3e6	1.2e6	1e-3	14	1.6e6	1.2e6	2.0e6	1.5e6	2	1.4e8	7.0e7	>3e8	1.5e7
1e-5	15	2.4e4	1.9e4	3.0e4	2.4e4	15	1.2e6	1.0e6	1.3e6	1.2e6	1e-5	14	1.6e6	1.2e6	2.0e6	1.5e6	2	1.4e8	7.0e7	>3e8	1.5e7
1e-8	15	2.5e4	1.9e4	3.0e4	2.5e4	15	1.2e6	1.0e6	1.3e6	1.2e6	1e-8	14	1.7e6	1.3e6	2.1e6	1.7e6	0	<i>14e-1</i>	<i>89e-9</i>	<i>32e-1</i>	8.9e6
$f_{115}$ in 5-D, N=15, mFE=69345					$f_{115}$ in 20-D, N=15, mFE=325587					$f_{116}$ in 5-D, N=15, mFE=77546					$f_{116}$ in 20-D, N=15, mFE=2.24e6						
10	15	1.1e2	9.6e1	1.3e2	1.1e2	15	5.2e3	4.6e3	5.8e3	5.2e3	10	15	5.7e3	3.5e3	8.1e3	5.7e3	15	5.0e5	3.9e5	6.1e5	5.0e5
1	15	2.0e3	3.0e2	3.7e3	2.0e3	15	3.8e4	2.1e4	5.4e4	3.8e4	1	15	1.4e4	9.3e3	2.0e4	1.4e4	15	6.9e5	5.5e5	8.3e5	6.9e5
1e-1	15	5.3e3	2.6e3	8.1e3	5.3e3	15	9.2e4	7.5e4	1.1e5	9.2e4	1e-1	15	2.2e4	1.6e4	2.9e4	2.2e4	15	8.9e5	7.4e5	1.0e6	8.9e5
1e-3	15	1.3e4	9.6e3	1.6e4	1.3e4	15	1.3e5	1.2e5	1.3e5	1.3e5	1e-3	15	2.7e4	2.1e4	3.3e4	2.7e4	15	1.2e6	1.0e6	1.4e6	1.2e6
1e-5	15	1.3e4	9.8e3	1.6e4	1.3e4	15	1.3e5	1.2e5	1.3e5	1.3e5	1e-5	15	3.0e4	2.5e4	3.6e4	3.0e4	15	1.5e6	1.5e6	1.6e6	1.5e6
1e-8	15	3.1e4	2.5e4	3.8e4	3.1e4	15	1.4e5	1.3e5	1.6e5	1.4e5	1e-8	15	3.2e4	2.7e4	3.9e4	3.2e4	15	1.6e6	1.5e6	1.7e6	1.6e6
$f_{117}$ in 5-D, N=15, mFE=5.01e6					$f_{117}$ in 20-D, N=15, mFE=2.00e7					$f_{118}$ in 5-D, N=15, m											

$f_{101}$ in 5-D, N=15, mFE=1072					$f_{101}$ in 20-D, N=15, mFE=13288					$f_{102}$ in 5-D, N=15, mFE=1093					$f_{102}$ in 20-D, N=15, mFE=13675						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	3.7e1	3.1e1	4.3e1	3.7e1	15	1.4e3	1.3e3	1.4e3	1.4e3	10	15	3.1e1	2.7e1	3.4e1	3.1e1	15	1.3e3	1.2e3	1.4e3	1.3e3
1	15	1.3e2	1.2e2	1.3e2	1.3e2	15	2.7e3	2.6e3	2.7e3	2.7e3	1	15	9.9e1	8.9e1	1.1e2	9.9e1	15	2.6e3	2.5e3	2.6e3	2.6e3
1e-1	15	2.2e2	2.2e2	2.3e2	2.2e2	15	4.0e3	3.9e3	4.0e3	4.0e3	1e-1	15	2.1e2	2.0e2	2.2e2	2.1e2	15	3.9e3	3.8e3	3.9e3	3.9e3
1e-3	15	4.4e2	4.3e2	4.5e2	4.4e2	15	6.5e3	6.5e3	6.6e3	6.5e3	1e-3	15	4.4e2	4.3e2	4.5e2	4.4e2	15	6.4e3	6.4e3	6.5e3	6.4e3
1e-5	15	6.6e2	6.5e2	6.8e2	6.6e2	15	9.1e3	9.0e3	9.2e3	9.1e3	1e-5	15	6.4e2	6.3e2	6.5e2	6.4e2	15	9.0e3	8.9e3	9.1e3	9.0e3
1e-8	15	9.7e2	9.6e2	9.9e2	9.7e2	15	1.3e4	1.3e4	1.3e4	1.3e4	1e-8	15	9.5e2	9.4e2	9.7e2	9.5e2	15	1.3e4	1.3e4	1.3e4	1.3e4
$f_{103}$ in 5-D, N=15, mFE=313583					$f_{103}$ in 20-D, N=15, mFE=3.18e6					$f_{104}$ in 5-D, N=15, mFE=2983					$f_{104}$ in 20-D, N=15, mFE=1.89e6						
10	15	3.0e1	2.5e1	3.6e1	3.0e1	15	1.3e3	1.3e3	1.4e3	1.3e3	10	15	2.5e2	2.2e2	2.9e2	2.5e2	15	7.7e5	6.3e5	9.2e5	7.7e5
1	15	1.2e2	1.2e2	1.3e2	1.2e2	15	2.5e3	2.4e3	2.6e3	2.5e3	1	15	7.7e2	6.5e2	9.0e2	7.7e2	15	8.2e5	6.7e5	9.8e5	8.2e5
1e-1	15	2.2e2	2.1e2	2.4e2	2.2e2	15	4.8e3	3.8e3	5.8e3	4.8e3	1e-1	15	1.3e3	1.2e3	1.4e3	1.3e3	15	8.4e5	6.9e5	1.0e6	8.4e5
1e-3	15	1.7e3	4.5e2	3.0e3	1.7e3	15	2.8e4	1.9e4	3.7e4	2.8e4	1e-3	15	1.8e3	1.7e3	1.9e3	1.8e3	15	8.6e5	7.0e5	1.0e6	8.6e5
1e-5	15	1.3e4	7.7e3	1.9e4	1.3e4	15	3.1e5	2.4e5	3.9e5	3.1e5	1e-5	15	2.0e3	1.9e3	2.2e3	2.0e3	15	8.7e5	7.1e5	1.0e6	8.7e5
1e-8	15	1.5e5	1.1e5	1.8e5	1.5e5	15	1.9e6	1.6e6	2.3e6	1.9e6	1e-8	15	2.4e3	2.3e3	2.5e3	2.4e3	15	8.8e5	7.3e5	1.0e6	8.8e5
$f_{105}$ in 5-D, N=15, mFE=47725					$f_{105}$ in 20-D, N=15, mFE=2.00e7					$f_{106}$ in 5-D, N=15, mFE=1.07e6					$f_{106}$ in 20-D, N=15, mFE=2.00e7						
10	15	2.4e2	2.3e2	2.6e2	2.4e2	15	2.8e8	1.3e8	>3e8	2.0e7	10	15	2.3e2	2.2e2	2.5e2	2.3e2	15	1.5e6	8.2e5	2.3e6	1.5e6
1	15	1.2e4	7.6e3	1.6e4	1.2e4	10	1.3e+0	1.0e+0	1.5e+0	1.0e7	1	15	4.8e3	2.7e3	7.2e3	4.8e3	2	1.3e8	7.0e7	>3e8	2.0e7
1e-1	15	1.5e4	1.1e4	1.9e4	1.5e4						1e-1	15	1.0e4	7.7e3	1.3e4	1.0e4	2	1.2e8	1.3e8	>3e8	2.0e7
1e-3	15	1.5e4	1.1e4	2.0e4	1.5e4						1e-3	15	3.3e4	2.3e4	4.5e4	3.3e4	0	47e-1	30e-2	81e-1	5.6e6
1e-5	15	1.6e4	1.2e4	2.0e4	1.6e4						1e-5	15	1.2e5	8.7e4	1.6e5	1.2e5					
1e-8	15	1.6e4	1.2e4	2.1e4	1.6e4						1e-8	15	1.5e5	4.0e5	6.2e5	5.1e5					
$f_{107}$ in 5-D, N=15, mFE=799012					$f_{107}$ in 20-D, N=15, mFE=4.30e6					$f_{108}$ in 5-D, N=15, mFE=5.01e6					$f_{108}$ in 20-D, N=15, mFE=2.00e7						
10	15	1.3e3	6.0e1	2.6e3	1.3e3	15	1.6e5	1.2e5	2.1e5	1.6e5	10	15	1.1e4	6.0e3	1.6e4	1.1e4	15	4.4e6	3.8e6	5.1e6	4.4e6
1	15	7.1e3	4.4e3	1.0e4	7.1e3	15	1.4e6	1.2e6	1.6e6	1.4e6	1	15	8.4e4	6.0e4	1.1e5	8.4e4	8	2.6e7	1.8e7	4.1e7	1.2e7
1e-1	15	1.3e4	9.8e3	1.6e4	1.3e4	15	1.5e6	1.3e6	1.7e6	1.5e6	1e-1	15	3.8e5	3.0e5	4.6e5	3.8e5	2	1.4e8	7.1e7	>3e8	2.0e7
1e-3	15	2.1e4	1.7e4	2.6e4	2.1e4	15	1.6e6	1.4e6	1.8e6	1.6e6	1e-3	15	1.3e6	1.0e6	1.6e6	1.3e6	0	85e-2	96e-3	23e-1	7.9e6
1e-5	15	3.1e4	2.4e4	3.8e4	3.1e4	15	2.0e6	1.7e6	2.3e6	2.0e6	1e-5	10	4.7e6	3.4e6	6.8e6	2.8e6					
1e-8	15	5.6e4	4.6e4	6.5e4	5.6e4	15	2.9e6	2.5e6	3.3e6	2.9e6	1e-8	3	2.4e7	1.5e7	7.3e7	5.0e6					
$f_{109}$ in 5-D, N=15, mFE=799091					$f_{109}$ in 20-D, N=15, mFE=3.62e6					$f_{110}$ in 5-D, N=15, mFE=5.01e6					$f_{110}$ in 20-D, N=15, mFE=2.00e7						
10	15	2.9e1	2.5e1	3.3e1	2.9e1	15	1.3e3	1.3e3	1.4e3	1.3e3	10	15	4.5e3	2.7e3	6.4e3	4.5e3	0	18e+0	18e+0	18e+0	8.9e6
1	15	1.3e2	1.2e2	1.4e2	1.3e2	15	5.4e3	2.8e3	8.1e3	5.4e3	1	15	3.0e5	2.1e5	4.0e5	3.0e5					
1e-1	15	3.5e3	1.1e3	6.5e3	3.5e3	15	2.3e4	1.5e4	3.0e4	2.3e4	1e-1	9	5.5e6	3.7e6	8.5e6	2.5e6					
1e-3	15	3.7e4	2.7e4	4.8e4	3.7e4	15	7.1e5	5.6e5	8.5e5	7.1e5	1e-3	6	1.0e7	6.6e6	1.8e7	3.2e6					
1e-5	15	1.6e5	1.3e5	1.8e5	1.6e5	15	1.5e6	1.3e6	1.8e6	1.5e6	1e-5	5	1.2e7	7.9e6	2.3e7	3.6e6					
1e-8	15	4.5e5	3.8e5	5.1e5	4.5e5	15	1.8e6	1.5e6	2.1e6	1.8e6	1e-8	4	1.5e7	9.2e6	3.4e7	3.3e6					
$f_{111}$ in 5-D, N=15, mFE=5.01e6					$f_{111}$ in 20-D, N=15, mFE=2.00e7					$f_{112}$ in 5-D, N=15, mFE=5.01e6					$f_{112}$ in 20-D, N=15, mFE=2.00e7						
10	15	4.9e4	4.0e4	5.9e4	4.9e4	10	27e+0	20e+0	35e+0	7.9e6	10	15	2.5e2	2.3e2	2.7e2	2.5e2	13	1.4e7	1.2e7	1.7e7	1.1e7
1	14	2.3e6	1.7e6	2.9e6	2.3e6						1	15	1.5e5	1.1e5	2.0e5	1.5e5	7	3.6e7	2.6e7	5.7e7	1.6e7
1e-1	3	2.2e7	1.3e7	6.7e7	5.0e6						1e-1	15	1.2e6	8.6e5	1.5e6	1.2e6	7	3.6e7	2.6e7	5.6e7	1.6e7
1e-3	0	26e-2	43e-3	64e-2	2.2e6						1e-3	15	1.9e6	1.6e6	2.3e6	1.9e6	7	3.6e7	2.6e7	5.6e7	1.6e7
1e-5											1e-5	15	2.2e6	1.9e6	2.6e6	2.2e6	7	3.6e7	2.6e7	5.5e7	1.6e7
1e-8											1e-8	13	3.6e6	2.9e6	4.3e6	3.0e6	7	3.6e7	2.6e7	5.5e7	1.6e7
$f_{113}$ in 5-D, N=15, mFE=83906					$f_{113}$ in 20-D, N=15, mFE=4.07e6					$f_{114}$ in 5-D, N=15, mFE=5.01e6					$f_{114}$ in 20-D, N=15, mFE=2.00e7						
10	15	1.3e2	1.1e2	1.6e2	1.3e2	15	2.6e5	1.9e5	3.3e5	2.6e5	10	15	8.1e3	5.8e3	1.0e4	8.1e3	13	8.8e6	6.7e6	1.1e7	7.9e6
1	15	8.8e3	3.4e3	1.5e4	8.8e3	15	1.6e6	1.4e6	1.8e6	1.6e6	1	15	2.1e5	1.6e5	2.7e5	2.1e5	1	2.9e8	1.4e8	>3e8	2.0e7
1e-1	15	3.4e4	2.4e4	4.4e4	3.4e4	15	2.3e6	2.0e6	2.6e6	2.3e6	1e-1	15	8.3e5	6.2e5	1.1e6	8.3e5	0	27e-1	11e-1	11e+0	7.9e6
1e-3	15	4.3e4	3.3e4	5.2e4	4.3e4	15	3.1e6	2.7e6	3.4e6	3.1e6	1e-3	12	3.5e6	2.7e6	4.7e6	2.6e6					
1e-5	15	4.3e4	3.3e4	5.2e4	4.3e4	15	3.1e6	2.7e6	3.4e6	3.1e6	1e-5	12	3.5e6	2.7e6	4.8e6	2.6e6					
1e-8	15	4.3e4	3.4e4	5.2e4	4.3e4	15	3.1e6	2.8e6	3.4e6	3.1e6	1e-8	12	3.6e6	2.7e6	4.7e6	2.7e6					
$f_{115}$ in 5-D, N=15, mFE=108673					$f_{115}$ in 20-D, N=15, mFE=1.16e6					$f_{116}$ in 5-D, N=15, mFE=153370					$f_{116}$ in 20-D, N=15, mFE=4.41e6						
10	15	9.9e1	8.8e1	1.1e2	9.9e1	15	3.2e3	2.3e3	4.1e3	3.2e3	10	15	2.3e4	1.7e4	2.9e4	2.3e4	15	1.9e6	1.6e6	2.2e6	1.9e6
1	15	2.0e3	8.7e2	3.4e3	2.0e3	15	5.2e4	3.3e4	7.3e4	5.2e4	1	15	4.7e4	3.3e4	6.0e4	4.7e4	15	2.0e6	1.7e6	2.4e6	2.0e6
1e-1	15	1.6e4	1.1e4	2.1e4	1.6e4	15	2.2e5	1.7e5	2.7e5	2.2e5	1e-1	15	5.6e4	4.4e4	7.0e4	5.6e4	15	2.2e6	1.9e6	2.6e6	2.2e6
1e-3	15	5.1e4	4.1e4	6.0e4	5.1e4	15	8.9e5	7.8e5	9.9e5	8.9e5	1e-3	15	6.3e4	5.1e4	7.6e4	6.3e4	15	2.6e6	2.2e6	3.0e6	2.6e6
1e-5	15	5.1e4	4.1e4	6.0e4	5.1e4	15	8.9e5	7.8e5	9.9e5	8.9e5	1e-5	15	7.8e4	6.6e4	9.0e4	7.8e4	15	2.6e6	2.3e6	3.0e6	2.6e6
1e-8	15	6.0e4	5.1e4	6.9e4	6.0e4	15	9.6e5	8.8e5	1.0e6	9.6e5	1e-8	15	8.6e4	7.6e4	9.6e4	8.6e4	15	2.9e6	2.5e6	3.3e6	2.9e6
$f_{117}$ in 5-D, N=15, mFE=5.01e6					$f_{117}$ in 20-D, N=15, mFE=2.00e7					$f_{118}$ in 5-D, N=15, mFE=756125					$f_{118}$ in 20-D, N=15, mFE=3.29e6						
10	15	1.2e5	8.3e4	1.5e5	1.2e5	4	6.4e7	4.1e7	1.3e8	1.7e7	10	15	1.2e3	2.9e2	2.1e3	1.2e3	15	1.			

$f_{121}$ in 5-D, N=15, mFE=2.71e6					$f_{121}$ in 20-D, N=15, mFE=3.04e6					$f_{122}$ in 5-D, N=15, mFE=733298					$f_{122}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.8e1	1.3e1	2.3e1	1.8e1	15	1.6e3	1.5e3	1.6e3	1.6e3	10	15	1.3e1	1.0e1	1.7e1	1.3e1	15	9.5e2	7.9e2	1.1e3	9.5e2
1	15	2.0e2	1.8e2	2.2e2	2.0e2	15	4.6e3	4.4e3	4.8e3	4.6e3	1	15	8.4e3	4.5e3	1.2e4	8.4e3	15	8.5e5	7.0e5	1.0e6	8.5e5
1e-1	15	3.3e3	6.7e2	6.0e3	3.3e3	15	6.7e4	4.6e4	8.9e4	6.7e4	1e-1	15	5.1e4	4.1e4	6.2e4	5.1e4	15	2.6e6	2.2e6	3.0e6	2.6e6
1e-3	15	4.1e4	3.0e4	5.3e4	4.1e4	15	2.3e5	1.9e5	2.7e5	2.3e5	1e-3	15	1.1e5	8.7e4	1.3e5	1.1e5	15	4.6e6	4.5e6	4.7e6	4.6e6
1e-5	15	1.6e5	1.3e5	2.0e5	1.6e5	15	5.1e5	3.9e5	6.2e5	5.1e5	1e-5	15	2.0e5	1.9e5	2.2e5	2.0e5	11	1.3e7	9.3e6	1.9e7	8.7e6
1e-8	15	9.7e5	7.5e5	1.2e6	9.7e5	15	1.2e6	1.1e6	1.4e6	1.2e6	1e-8	15	3.7e5	3.0e5	4.5e5	3.7e5	7	3.2e7	2.2e7	5.2e7	1.3e7
$f_{123}$ in 5-D, N=15, mFE=5.01e6					$f_{123}$ in 20-D, N=15, mFE=2.00e7					$f_{124}$ in 5-D, N=15, mFE=3.18e6					$f_{124}$ in 20-D, N=15, mFE=5.04e6						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	2.0e1	1.4e1	2.6e1	2.0e1	15	2.0e3	1.4e3	2.6e3	2.0e3	10	15	2.0e1	1.6e1	2.4e1	2.0e1	15	8.8e2	7.8e2	9.9e2	8.8e2
1	15	1.4e5	9.2e4	1.9e5	1.4e5	1	2.9e8	1.4e8	>3e8	2.0e7	1	15	5.0e3	2.3e3	7.8e3	5.0e3	15	2.1e4	1.0e4	3.1e4	2.1e4
1e-1	5	1.2e7	7.4e6	2.2e7	3.4e6	0	23e-1	12e-1	32e-1	8.9e6	1e-1	15	1.5e4	1.1e4	2.0e4	1.5e4	15	1.4e5	1.3e5	1.4e5	1.4e5
1e-3	0	15e-2	74e-3	17e-2	2.2e6	.	.	.	.	.	1e-3	15	2.0e5	1.6e5	2.5e5	2.0e5	15	5.8e5	4.6e5	6.9e5	5.8e5
1e-5	.	.	.	.	.	.	.	.	.	.	1e-5	15	8.5e5	7.2e5	9.8e5	8.5e5	15	1.3e6	1.0e6	1.6e6	1.3e6
1e-8	.	.	.	.	.	.	.	.	.	.	1e-8	15	1.9e6	1.6e6	2.2e6	1.9e6	15	2.0e6	1.5e6	2.5e6	2.0e6
$f_{125}$ in 5-D, N=15, mFE=5.01e6					$f_{125}$ in 20-D, N=15, mFE=2.00e7					$f_{126}$ in 5-D, N=15, mFE=5.01e6					$f_{126}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.1e0	1.0e0	1.1e0	1.1e0	15	1.1e0	1.0e0	1.3e0	1.1e0	10	15	1.0e0	1.0e0	1.0e0	1.0e0	15	1.0e0	1.0e0	1.0e0	1.0e0
1	15	3.7e1	2.9e1	4.5e1	3.7e1	15	1.0e3	9.4e2	1.1e3	1.0e3	1	15	4.5e1	3.7e1	5.3e1	4.5e1	15	1.3e3	1.2e3	1.4e3	1.3e3
1e-1	15	6.8e3	3.9e3	1.0e4	6.8e3	0	24e-2	15e-2	28e-2	1.4e7	1e-1	15	3.0e4	1.8e4	4.4e4	3.0e4	0	31e-2	29e-2	33e-2	8.9e6
1e-3	12	3.1e6	2.3e6	4.1e6	2.3e6	.	.	.	.	.	1e-3	0	15e-3	11e-3	28e-3	1.4e6	.	.	.	.	.
1e-5	9	5.5e6	4.0e6	8.0e6	3.1e6	.	.	.	.	.	1e-5	.	.	.	.	.	.	.	.	.	.
1e-8	9	5.5e6	4.0e6	8.1e6	3.1e6	.	.	.	.	.	1e-8	.	.	.	.	.	.	.	.	.	.
$f_{127}$ in 5-D, N=15, mFE=5.01e6					$f_{127}$ in 20-D, N=15, mFE=2.00e7					$f_{128}$ in 5-D, N=15, mFE=2.12e6					$f_{128}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.1e0	1.0e0	1.3e0	1.1e0	15	1.1e0	1.0e0	1.3e0	1.1e0	10	15	1.4e2	1.0e2	1.7e2	1.4e2	15	2.2e6	1.7e6	2.7e6	2.2e6
1	15	4.0e1	3.4e1	4.6e1	4.0e1	15	7.6e2	7.1e2	8.0e2	7.6e2	1	15	2.0e5	1.2e5	2.7e5	2.0e5	11	1.6e7	1.2e7	2.1e7	1.2e7
1e-1	15	2.7e3	7.0e2	4.7e3	2.7e3	15	1.5e6	9.7e5	2.0e6	1.5e6	1e-1	15	3.6e5	2.0e5	5.4e5	3.6e5	10	1.8e7	1.3e7	2.5e7	1.2e7
1e-3	14	1.8e6	1.4e6	2.2e6	1.7e6	0	83e-4	36e-4	40e-3	2.0e7	1e-3	15	3.7e5	2.0e5	5.4e5	3.7e5	10	1.8e7	1.4e7	2.5e7	1.2e7
1e-5	9	5.3e6	4.1e6	7.4e6	3.4e6	.	.	.	.	.	1e-5	15	3.7e5	2.1e5	5.5e5	3.7e5	10	1.9e7	1.4e7	2.5e7	1.2e7
1e-8	5	1.2e7	8.5e6	2.2e7	4.6e6	.	.	.	.	.	1e-8	15	3.8e5	2.1e5	5.6e5	3.8e5	10	1.9e7	1.4e7	2.6e7	1.3e7
$f_{129}$ in 5-D, N=15, mFE=5.00e6					$f_{129}$ in 20-D, N=15, mFE=2.00e7					$f_{130}$ in 5-D, N=15, mFE=3.52e6					$f_{130}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.8e2	1.4e2	2.1e2	1.8e2	2	1.4e8	7.3e7	>3e8	2.0e7	10	15	1.1e2	9.6e1	1.3e2	1.1e2	15	3.5e4	4.8e3	6.5e4	3.5e4
1	15	2.1e5	1.3e5	2.9e5	2.1e5	1	2.9e8	1.4e8	>3e8	2.0e7	1	15	1.3e5	6.6e4	1.9e5	1.3e5	8	2.0e7	1.4e7	3.0e7	1.3e7
1e-1	15	6.9e5	3.9e5	1.0e6	6.9e5	0	23e+0	26e-1	28e+0	1.1e7	1e-1	15	4.2e5	1.5e5	7.2e5	4.2e5	8	2.1e7	1.4e7	3.0e7	1.3e7
1e-3	15	1.4e6	9.3e5	1.9e6	1.4e6	.	.	.	.	.	1e-3	15	4.3e5	1.7e5	7.1e5	4.3e5	8	2.1e7	1.5e7	3.1e7	1.3e7
1e-5	15	1.7e6	1.2e6	2.1e6	1.7e6	.	.	.	.	.	1e-5	15	4.9e5	2.2e5	8.1e5	4.9e5	8	2.1e7	1.5e7	3.1e7	1.3e7
1e-8	12	3.0e6	2.2e6	4.1e6	2.3e6	.	.	.	.	.	1e-8	15	5.7e5	2.7e5	8.8e5	5.7e5	8	2.2e7	1.6e7	3.2e7	1.3e7

Table 3: AMaLGaM: Shown are, for functions  $f_{121}$ - $f_{130}$  and for a given target difference to the optimal function value  $\Delta f$ : the number of successful trials (#); the expected running time to surpass  $f_{\text{opt}} + \Delta f$  (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (RT<sub>succ</sub>). If  $f_{\text{opt}} + \Delta f$  was never reached, figures in *italics* denote the best achieved  $\Delta f$ -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.

$f_{121}$ in 5-D, N=15, mFE=3.09e6					$f_{121}$ in 20-D, N=15, mFE=3.60e6					$f_{122}$ in 5-D, N=15, mFE=2.00e6					$f_{122}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.9e1	1.3e1	2.5e1	1.9e1	15	8.5e2	7.9e2	9.1e2	8.5e2	10	15	1.3e1	9.4e0	1.7e1	1.3e1	15	6.9e2	5.7e2	8.3e2	6.9e2
1	15	1.2e2	1.1e2	1.3e2	1.2e2	15	9.5e3	6.5e3	1.2e4	9.5e3	1	15	2.1e4	1.3e4	2.9e4	2.1e4	15	2.3e6	2.0e6	2.6e6	2.3e6
1e-1	15	1.5e3	3.4e2	2.8e3	1.5e3	15	8.2e4	4.2e4	1.2e5	8.2e4	1e-1	15	1.4e5	1.0e5	1.5e5	1.3e5	15	4.4e6	3.8e6	5.1e6	4.4e6
1e-3	15	7.8e4	5.6e4	1.0e5	7.8e4	15	1.1e6	9.2e5	1.4e6	1.1e6	1e-3	15	2.1e5	1.9e5	2.3e5	2.1e5	15	8.3e6	7.4e6	9.1e6	8.3e6
1e-5	15	4.4e5	3.8e5	5.1e5	4.4e5	15	1.7e6	1.5e6	2.0e6	1.7e6	1e-5	15	3.1e5	2.5e5	3.7e5	3.1e5	8	2.8e7	2.1e7	4.1e7	1.5e7
1e-8	15	1.6e6	1.4e6	1.9e6	1.6e6	15	2.3e6	2.0e6	2.6e6	2.3e6	1e-8	15	5.3e5	3.9e5	6.9e5	5.3e5	1	2.9e8	1.4e8	>3e8	2.0e7
$f_{123}$ in 5-D, N=15, mFE=5.01e6					$f_{123}$ in 20-D, N=15, mFE=2.00e7					$f_{124}$ in 5-D, N=15, mFE=5.01e6					$f_{124}$ in 20-D, N=15, mFE=1.24e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	2.4e1	1.2e1	3.7e1	2.4e1	15	1.3e4	5.6e3	2.0e4	1.3e4	10	15	1.1e1	7.4e0	1.4e1	1.1e1	15	5.4e2	4.5e2	6.1e2	5.4e2
1	15	3.0e5	2.4e5	3.6e5	3.0e5	0	23e-1	13e-1	43e-1	8.9e6	1	15	3.0e3	1.7e3	4.3e3	3.0e3	15	1.5e4	1.1e4	2.0e4	1.5e4
1e-1	5	1.3e7	9.1e6	2.3e7	4.8e6	.	.	.	.	.	1e-1	15	4.2e4	3.5e4	4.9e4	4.2e4	15	7.6e5	6.3e5	8.9e5	7.6e5
1e-3	0	18e-2	34e-3	24e-2	3.5e6	.	.	.	.	.	1e-3	15	3.5e5	2.8e5	4.3e5	3.5e5	15	2.2e6	1.9e6	2.5e6	2.2e6
1e-5	.	.	.	.	.	.	.	.	.	.	1e-5	14	2.6e6	2.1e6	3.1e6	2.4e6	15	2.4e6	2.1e6	2.7e6	2.4e6
1e-8	.	.	.	.	.	.	.	.	.	.	1e-8	13	3.4e6	2.8e6	4.0e6	3.0e6	15	3.5e6	2.8e6	4.3e6	3.5e6
$f_{125}$ in 5-D, N=15, mFE=5.01e6					$f_{125}$ in 20-D, N=15, mFE=2.00e7					$f_{126}$ in 5-D, N=15, mFE=5.01e6					$f_{126}$ in 20-D, N=15, mFE=2.00e7						
$\Delta f$	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	#	ERT	10%	90%	RT <sub>succ</sub>	
10	15	1.2e0	1.1e0	1.3e0	1.2e0	15	1.1e0	1.0e0	1.1e0	1.1e0	10										